

Hydrogen Spray Simulation with a Hollow-Cone Injector

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} Experimental team



Outline

- Background and Research Objective
- Experimental and Computational Setups
- Computational Validations
 - Qualitative Comparison
 - H₂ Jet Area and Penetration Length
 - Impact of Needle Lift
 - Shock Wave Prediction
 - Mass Flow Rate
- Conclusions



Background

Hydrogen is a promising green fuel for future transportation. The **direct-injection** hydrogen-fueled internal combustion engine (DI-H₂ ICE) has been viewed as one of the efficient transportation solutions, especially for heavy-duty applications.

Advantages of DI-H₂ in ICEs

- High volumetric efficiency and power density.
- No backfire and pre-ignition.
- High engine combustion efficiency.

Challenges

- High-pressure supersonic injection.
- Rapid fuel-air mixing in a confined chamber.
- Few usable measured data for high-fidelity modeling.

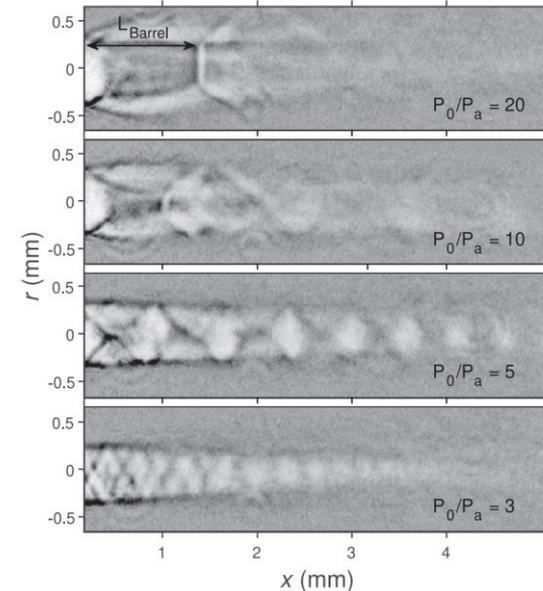


Fig. Near-field H₂ jet behavior at different reservoir pressure ratios¹.

Research Objective

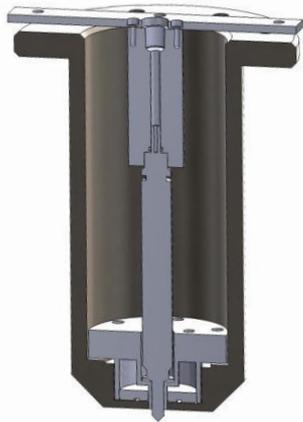
Work in Progress

1. Configure numerical models to adequately predict the H₂ jet behavior at different pressures (subcritical and supercritical).
2. Resolve the real injector geometry with a proper mesh to effectively and efficiently perform simulations.
3. Analyze the H₂ jet dynamics and identify the optimum solution to obtain the expected fuel-air mixing distribution.
4. Investigate the effects of nozzle geometry variation, inlet and ambient boundary conditions, and jet/wall interaction on the jet evolution process.



Constant Volume Chamber in KAUST

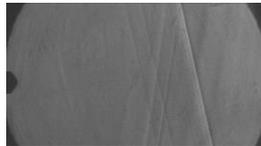
High-Pressure CVC



HDEV4 fixture



Z-type schlieren;
Pulsed LED;
30 and 100 K fps



Ambient content: N₂ at 2bar
Injected fuel: H₂ at 11bar

Test matrix

Parameters	Value
Hydrogen purity	> 99.98%
Hydrogen temperature [K]	298
Injection pressure [bar]	10, 20, 30, 40, and 50
Ambient pressure [bar]	1, 5, and 10
Ambient density [kg/m ³]	1.13, 5.65, and 11.32
Ambient temperature [K]	298
Injection duration [ms]	1 – 5

Bosch Hollow-Cone Injector

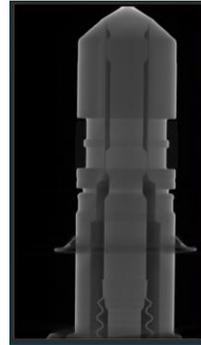


Technical features

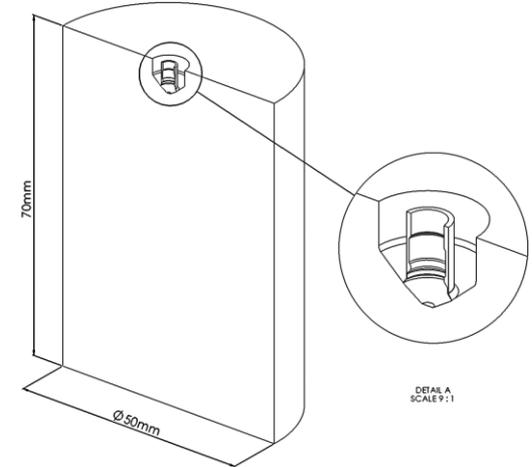
Needle actuation	Direct
Spray angle	$85^\circ \pm 5^\circ$
Shot-to-shot scatter	$\pm 1^\circ$
Back-pressure dependence	$< 4\%$
Resistance to carbon buildup	$< 3^\circ$
Droplet size SMD (Sauter Mean Diameter)	10–15 μm
Penetration	$< 30\text{ mm}$
System pressure	20 MPa
Needle lift	$\leq 35\ \mu\text{m}$
Dynamic flow range q_{dyn}	34.5 mg/lift @ $t_l = 1\text{ ms}$
Partial-lift capability	$\geq 10\text{--}35\ \mu\text{m}$
Injection time	70–5,000 μs
Multiple injection	≤ 5 injections/cycle
Interval time	$\geq 50\ \mu\text{s}$
Metering range	0.5–150 mg/injection



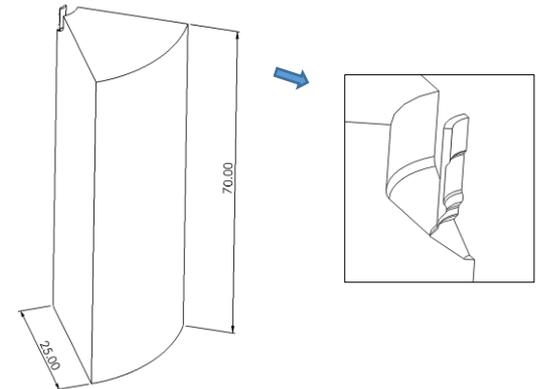
1 μm resolution



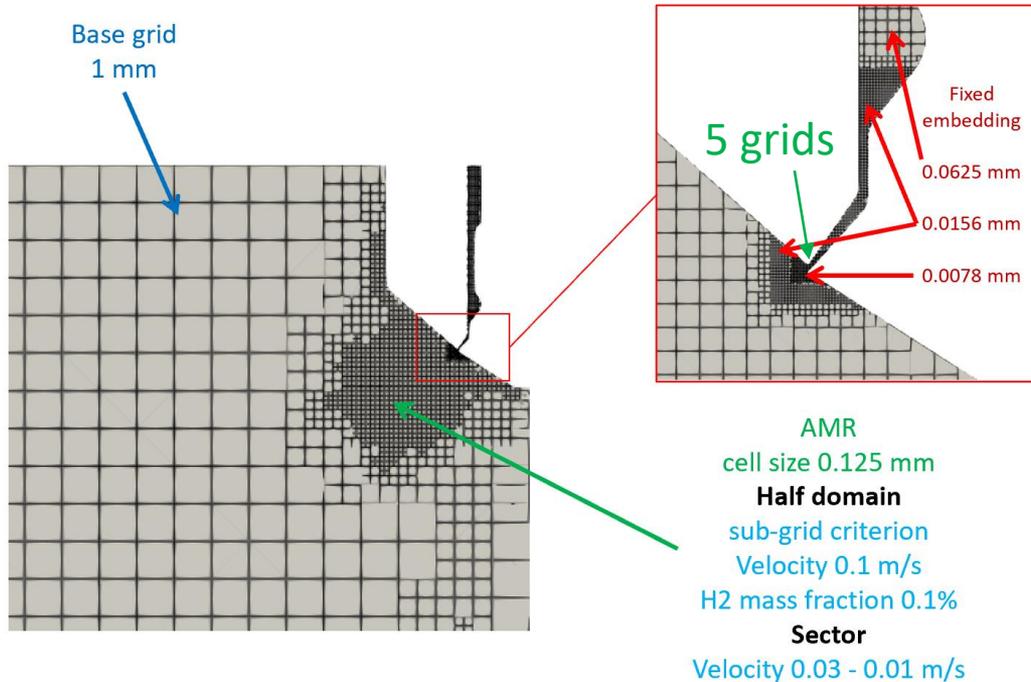
Half domain



60° sector



Mesh Details and Boundary Conditions



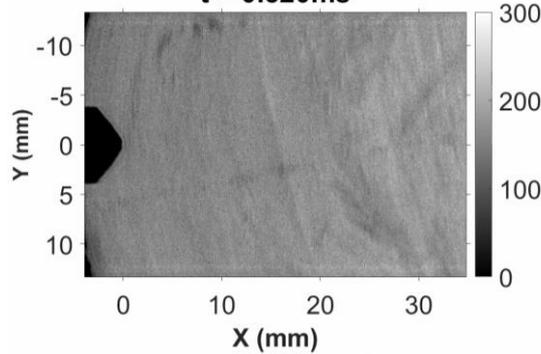
Fuel	H ₂
Ambient gas	N ₂
Injection pressure (bar)	11, 21, 51
Ambient pressure (bar)	2
Injection and ambient temperature (K)	298.15
Equation of state	Redlich-Kwong
Injector type	Hollow cone
Simulation type	Eulerian
Simulation duration (ms)	2

- CONVERGE 3.1 for CFD modeling.
- Turbulence model: RNG k - ϵ .

Qualitative Comparison – Jet Evolution

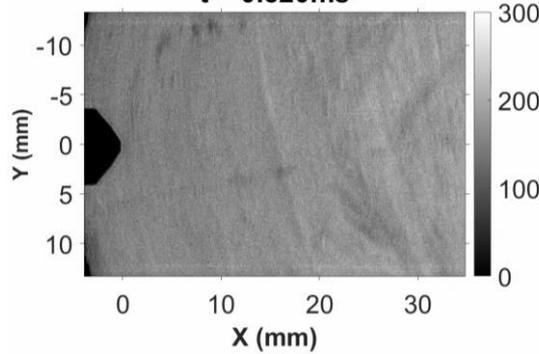
$P_{inj} = 11$ bar

$t = 0.520$ ms



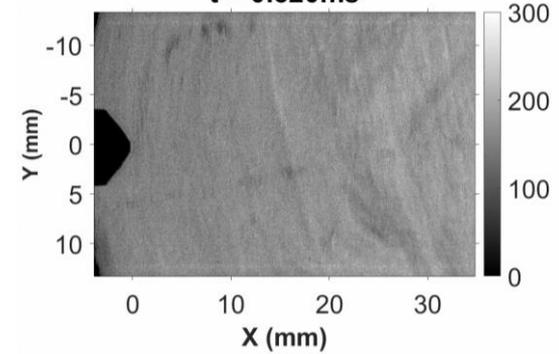
$P_{inj} = 21$ bar

$t = 0.520$ ms



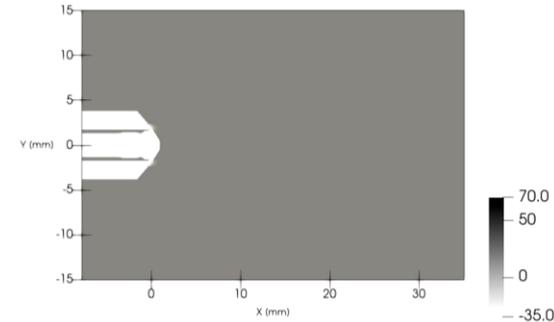
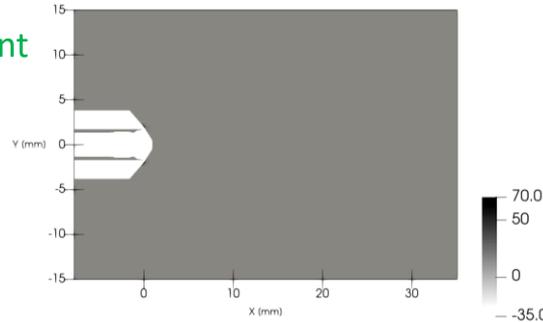
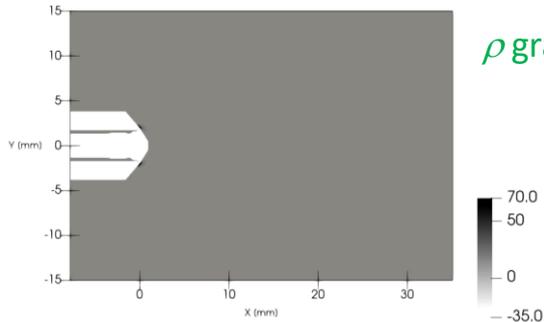
$P_{inj} = 51$ bar

$t = 0.520$ ms



Experiment
Z-type schlieren

ρ gradient

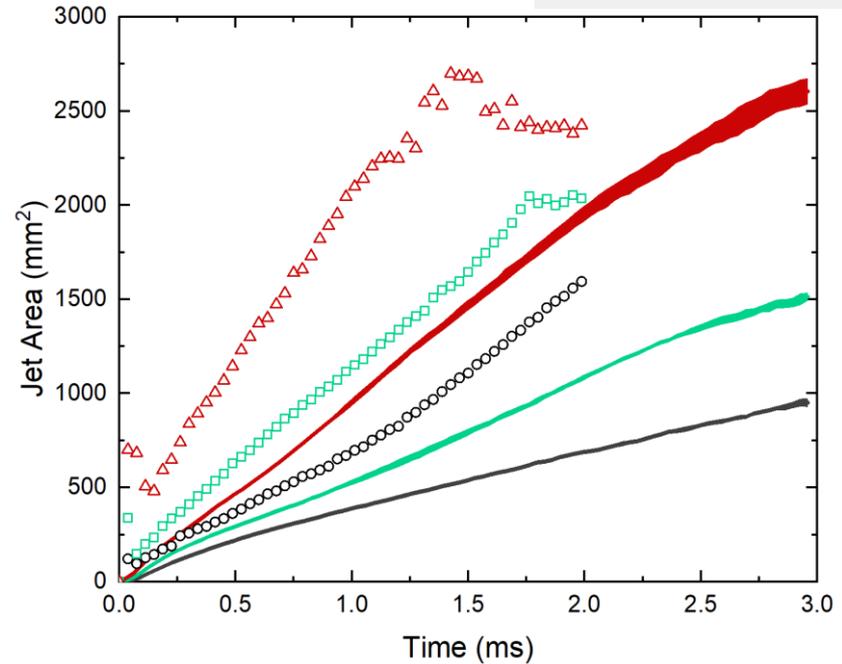
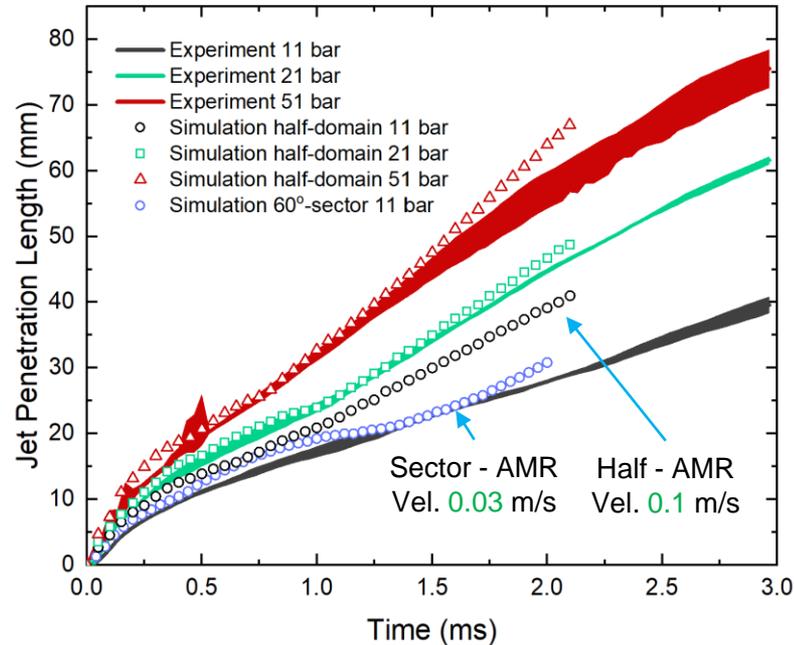
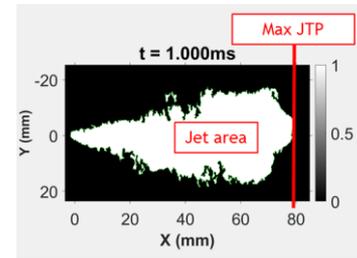


Simulation
Plane schlieren



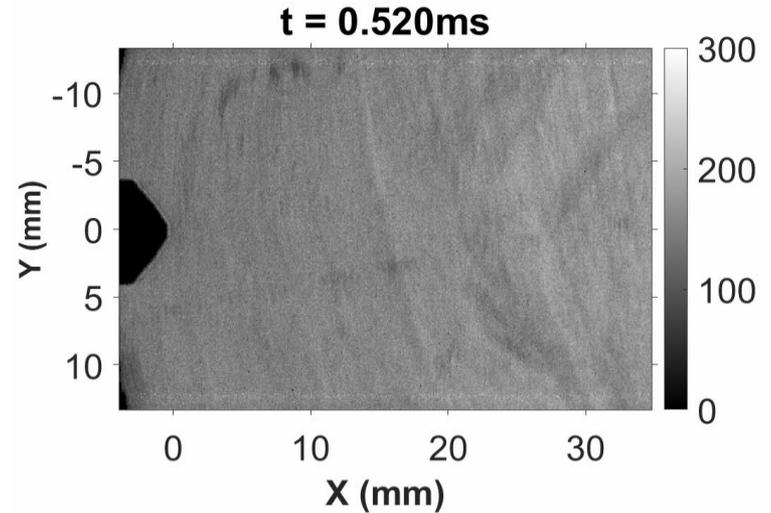
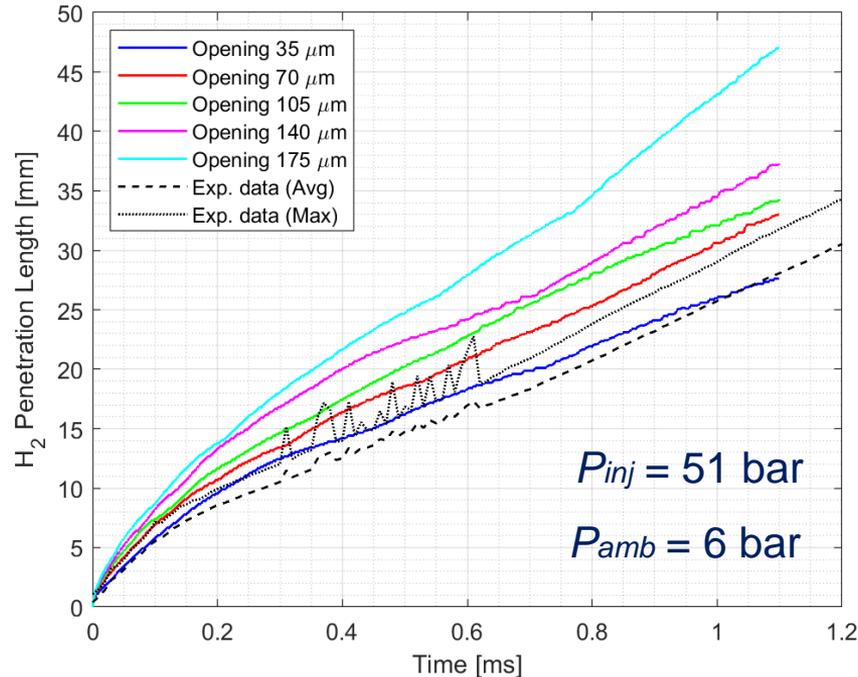
- Jet initiation delay due to hydraulic delay and starting video
- The predicted fields are overall reasonable.

Jet Penetration and Area



- Jet penetrations could be reasonably reproduced with a very fine AMR velocity sub-grid criterion.
- Jet area still existed a large discrepancy that should be resolved.

Impact of Needle Lift



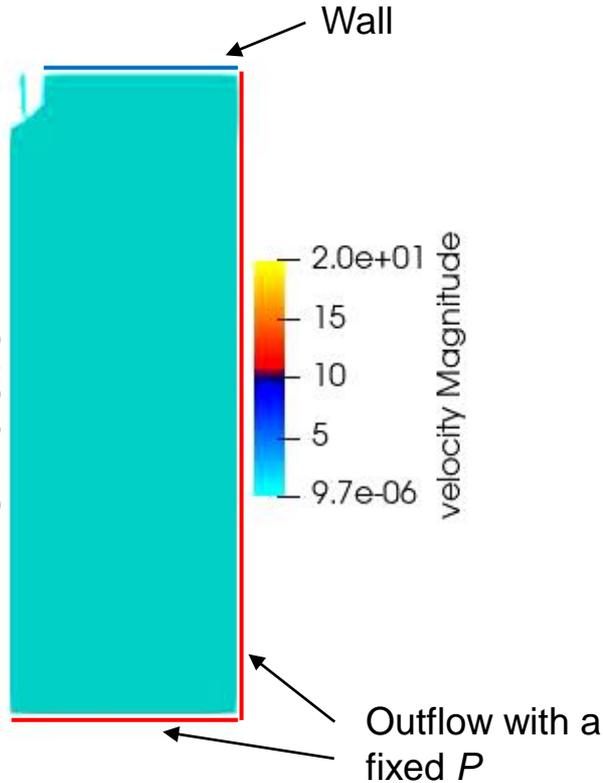
- Penetration increases with a higher needle lift.

Shock Wave Observation

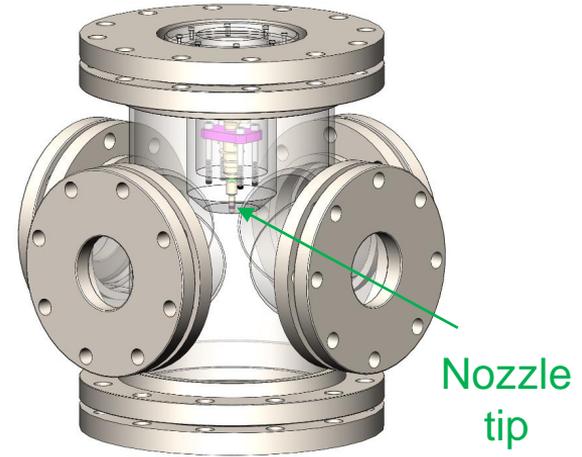
Experiment



Plane of 60° sector
simulation

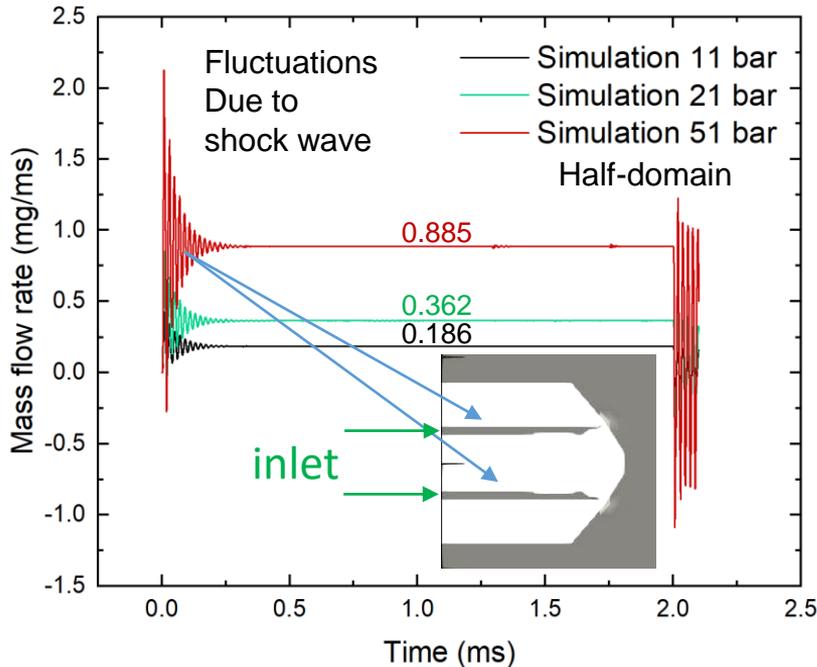


CVC test kit

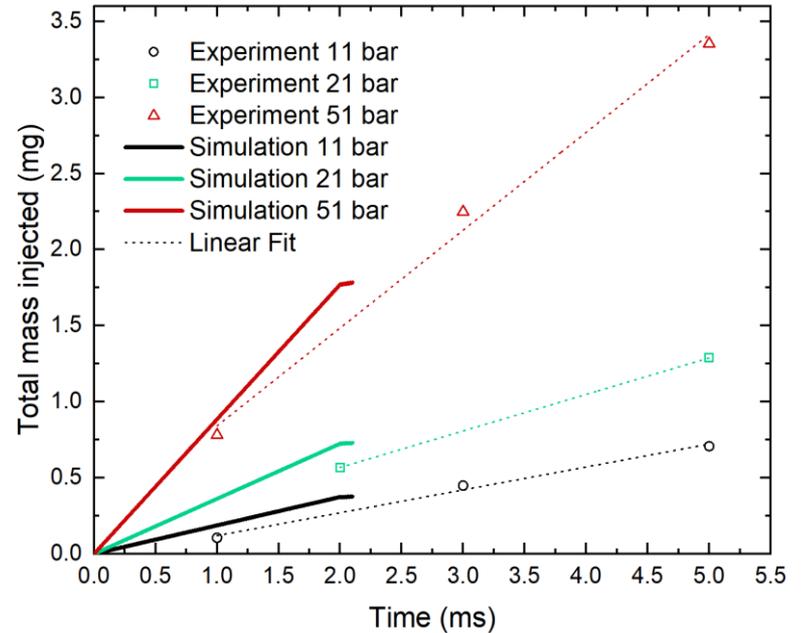


- Wave reflection issue in outflow possibly due to boundary setup. 11

Mass Flow Rate and Fuel Consumption



Integrated



- Initial pressure difference between two regions led to shock, which induced pressure fluctuation on the inlet boundary.
- Maybe more data from experiment needed to ensure more accurate slope.

Conclusions

1. For H₂ jet simulation using a hollow-cone injector, a precisely-measured nozzle geometry is significant in reproducing the measured jet metrics.
2. The predicted jet penetration is very sensitive to the mesh setup, especially near the nozzle exit region. A finer AMR sub-grid criterion resulted in the better agreement with measured data.
3. Injection pressure, needle lift, and start of injection timing are three of the most significant parameters that affect the prediction of jet penetration.
4. The outflow boundary with a fixed pressure condition yielded shock wave reflection, which should be resolved by properly setting up the outlet or wall boundary condition.



شكراً

THANK YOU!

Question?



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