

EFC Topic 4.4 Exploring CCV origin

Presented by Cecile PERA (IFPEN)

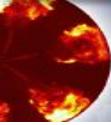
Objectives of the 4.4

Summarize: CCV understanding & modeling



TECHNISCHE
UNIVERSITÄT
DARMSTADT





Contributions

1. Motored operation

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2. Fired operation,

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Unimore

Czech Technical U

Convergent Science

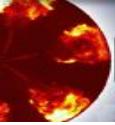
3. New tool modeling,

Cecile Pera, cecile.pera@ifpen.fr

IFPEN

4. Perspective,

All

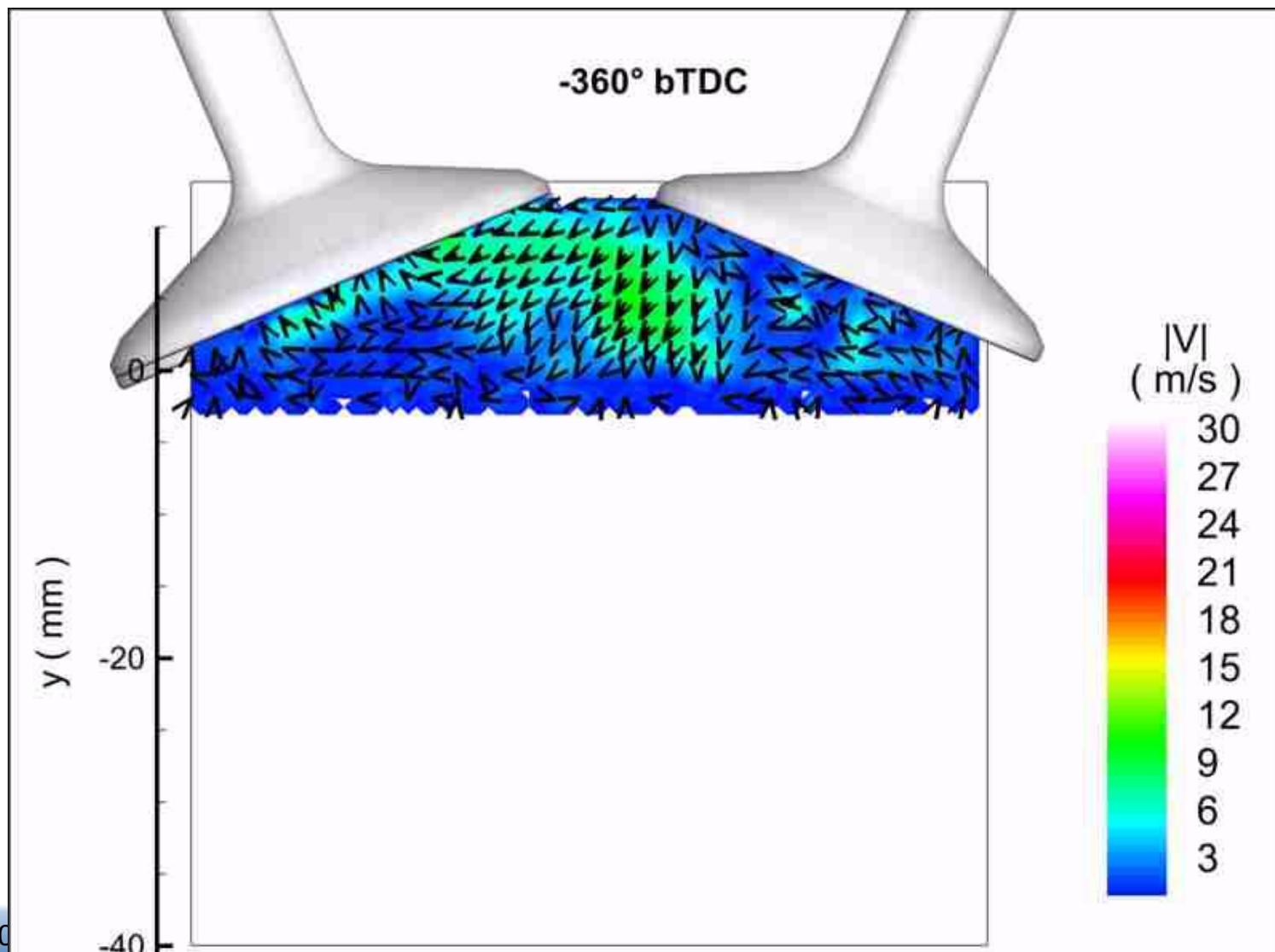


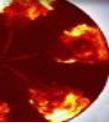
1. Motored operation



Instantaneous Flow Field (SIDI TU Darmstadt)

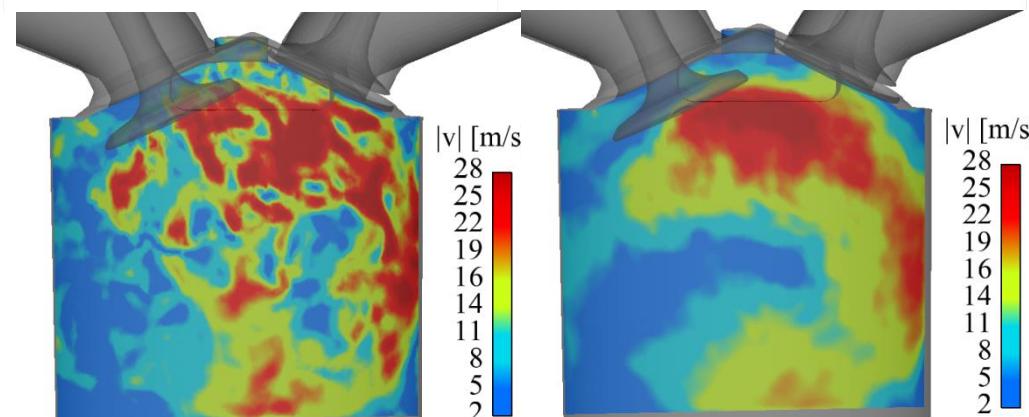
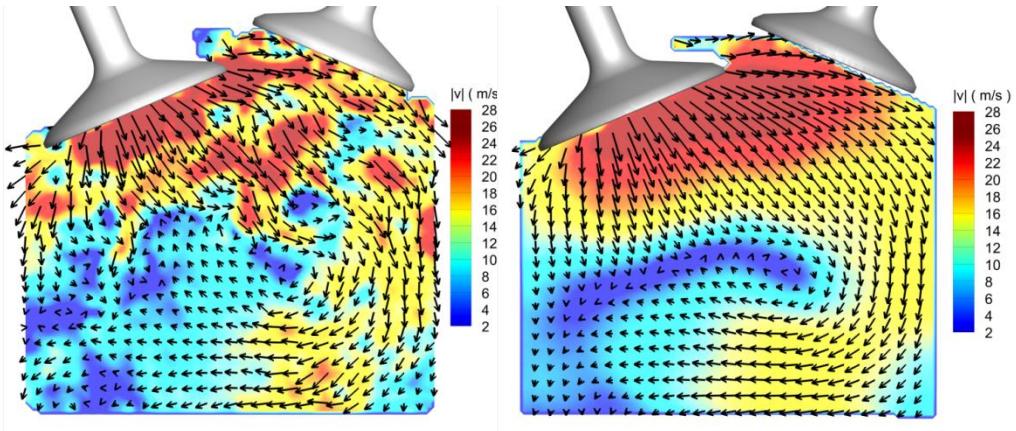
PIV measurements



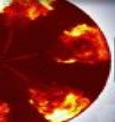


Instantaneous vs. Ensemble-Avg Flow Field

Instantaneous Ensemble-Avg



- How can we understand motored-CCVs?
- What is defined CCVs.
- Differences and roles of:
 - Large scale flow pattern
 - Turbulence



Velocity fluctuations

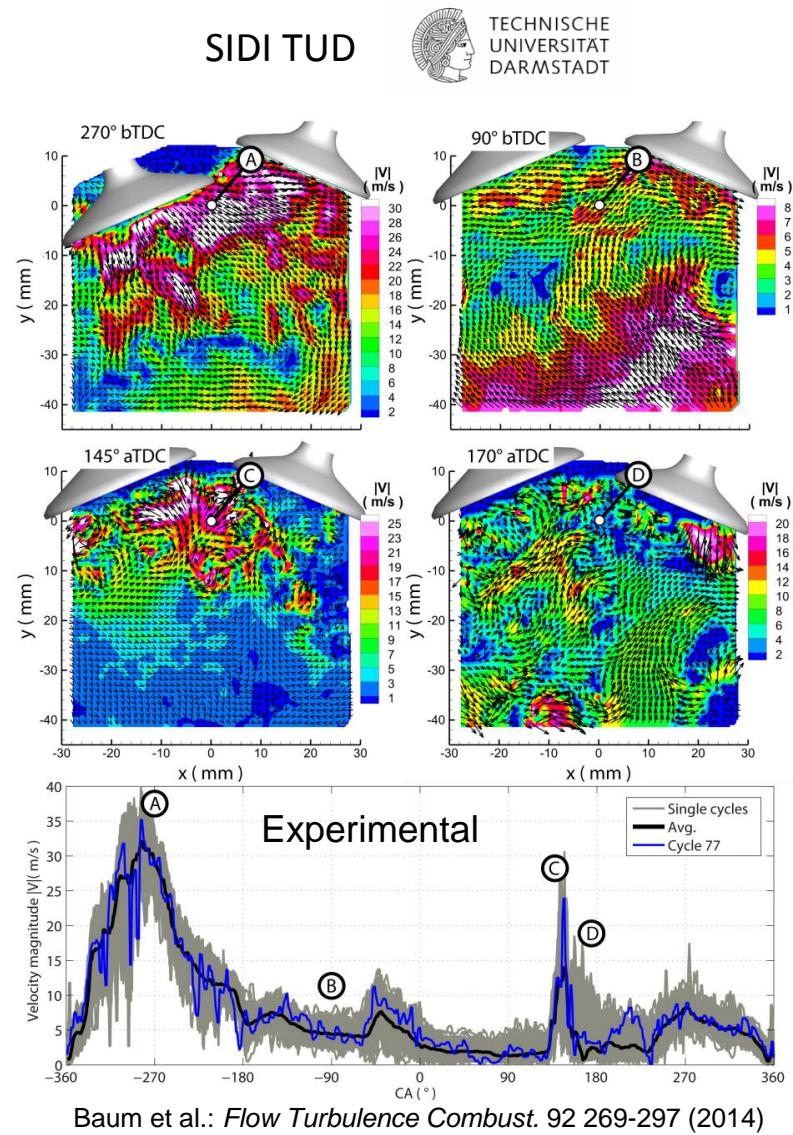
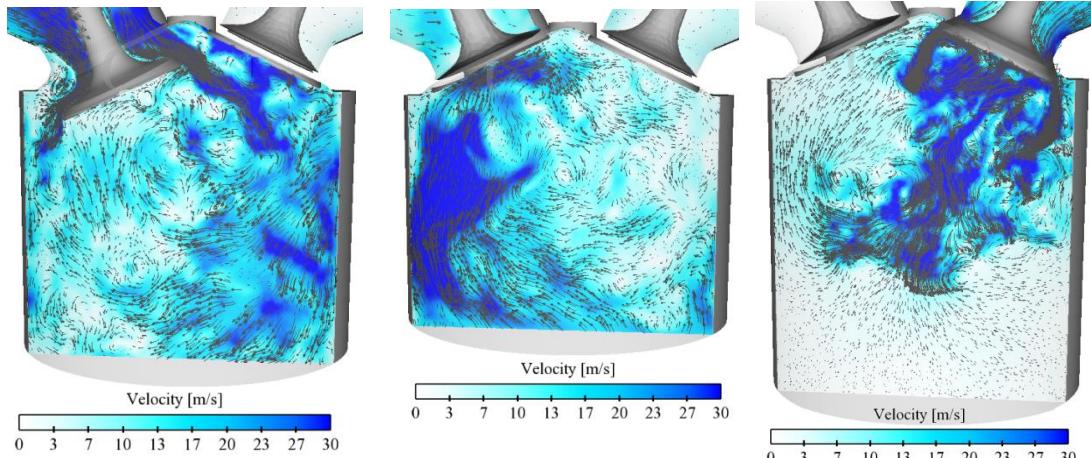
- Extract velocity at single point
- Entire engine cycle
 - High-speed PIV
- Deviations of inst. velocity from ensemble-average
- Large fluctuations throughout entire cycle

SGEmac LES IFP Energies nouvelles

-250 CAD

-100 CAD

145 CAD





Fluctuation of Large-Scale Flow Structures

PIV measurements



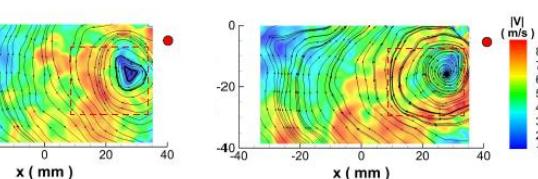
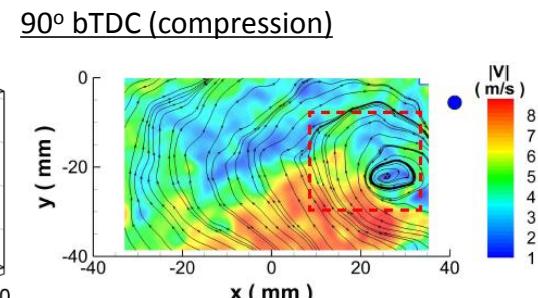
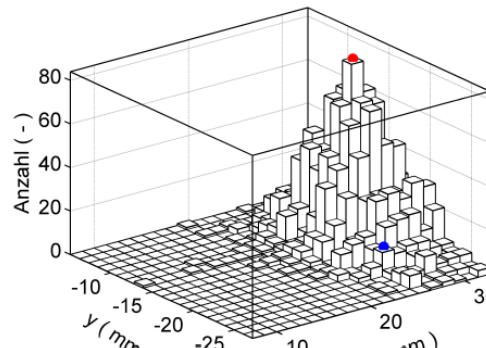
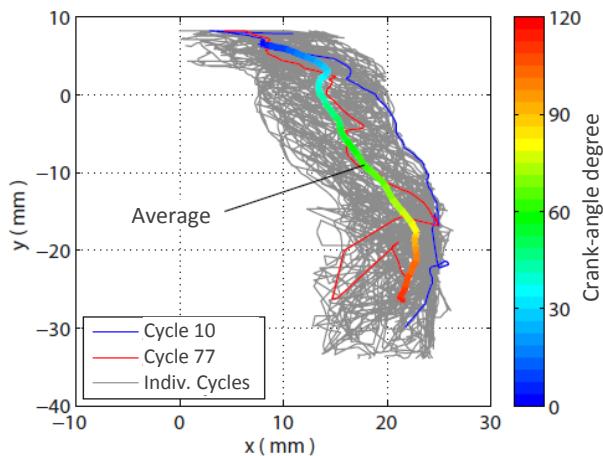
■ Identify tumble vortex

- Instantaneous images

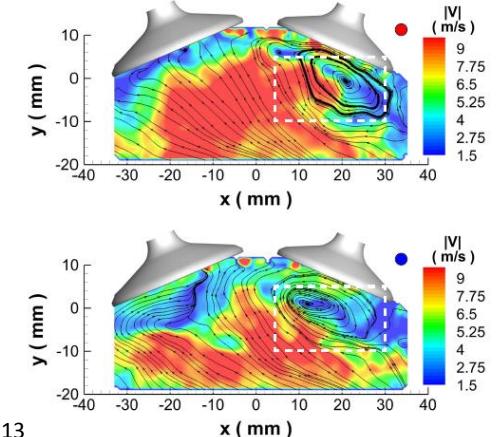
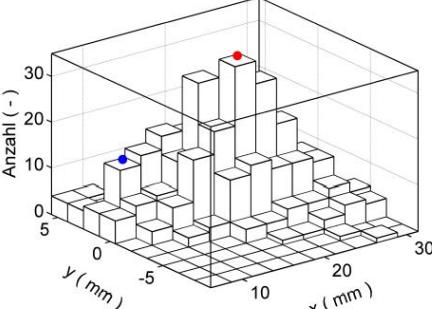
■ Location of maximal occurrence

■ Conditional sampling

- Formation of flow structures
- Cause of flow deviation
- High statistic needed
- Time history needed

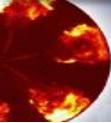


45° bTDC (compression)



Elias Baum, PhD Dissertation TU Darmstadt 2013



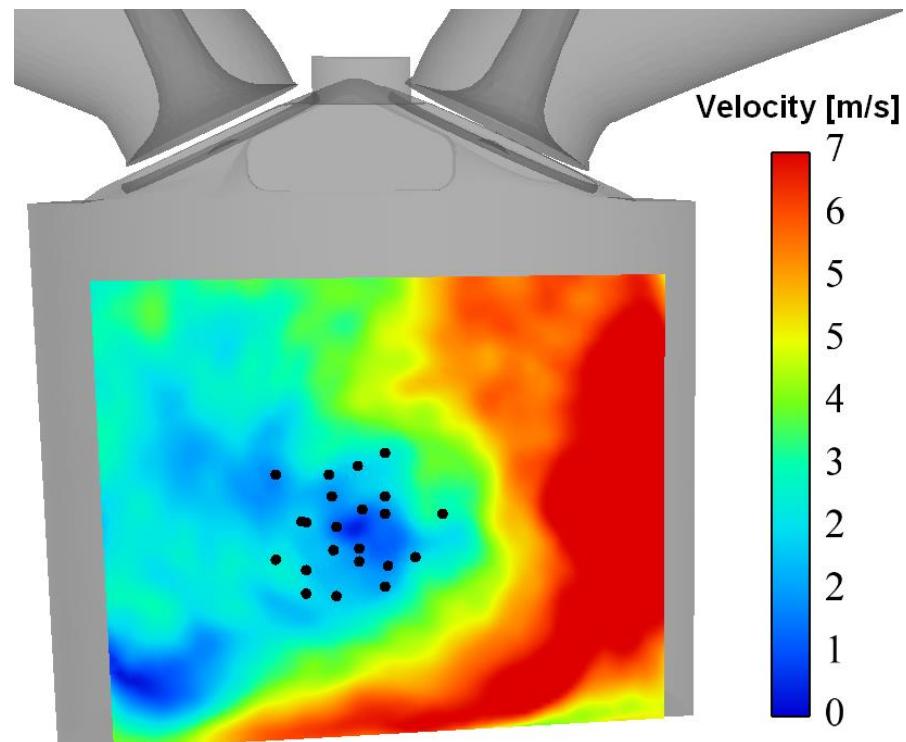
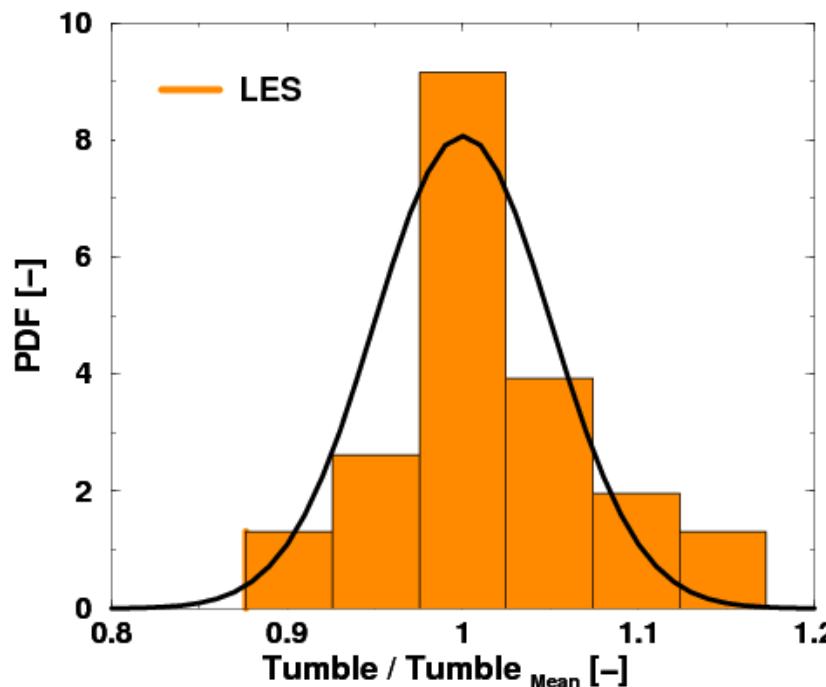


Fluctuation of Large-Scale Flow Structures (SGEmac IFP)

LES computations



- CCVs in spatial location of tumble motion
- CCVs in intensity of tumble motion





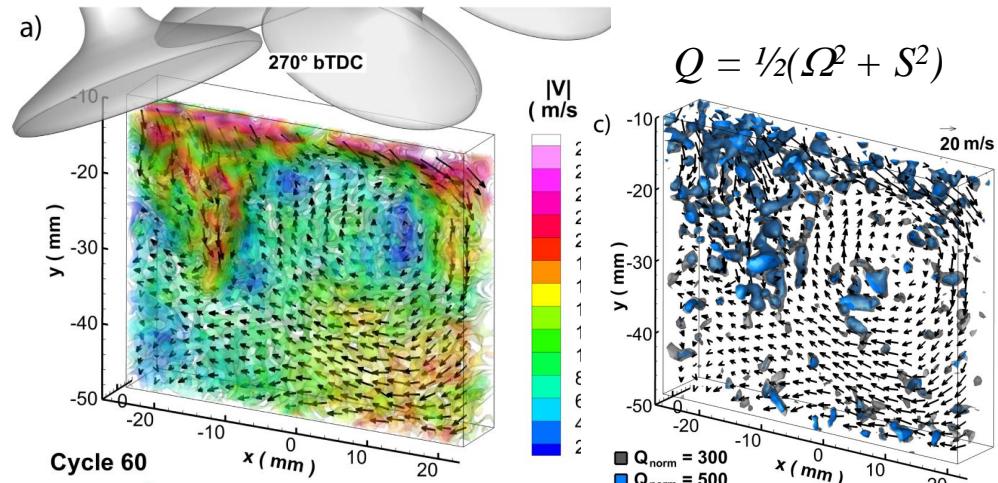
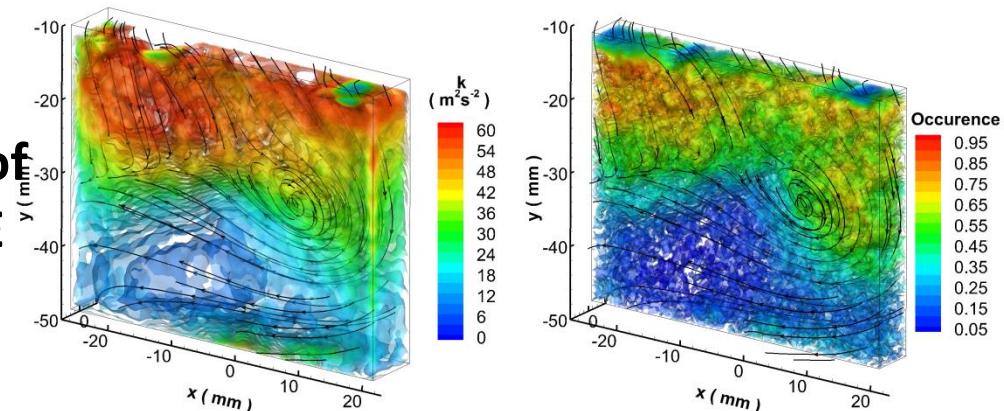
Turbulence Fluctuations vs Flow Variation

Tomographic PIV



- Tomographic PIV
- Identify 3D vortical structures
 - Q-criterion: $Q = 1/2 (\Omega^2 + S^2)$
- Probable location of 3D vortical structures
 - Topology
- Comparison to 3D TKE topology
 - Agreement: large influence of 3D vortical structures on TKE
 - Differences: TKE influence

Tomographic PIV, Instantaneous cycle 270° bTDC

Baum et al.: *Flow Turbulence Combust.* 92, 269-297 (2014)



Influence of Intake Flow

Magnetic Resonance Velocimetry (MRV)



■ Ensemble-average volumetric flow

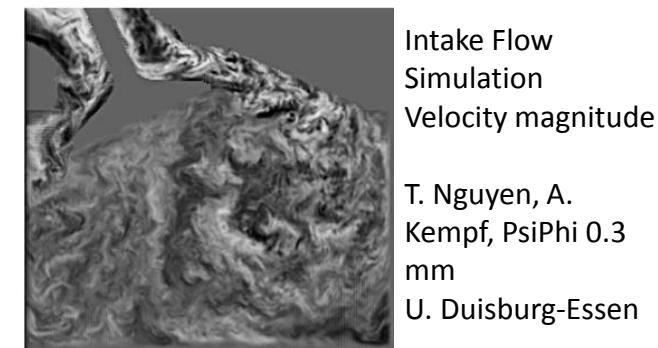
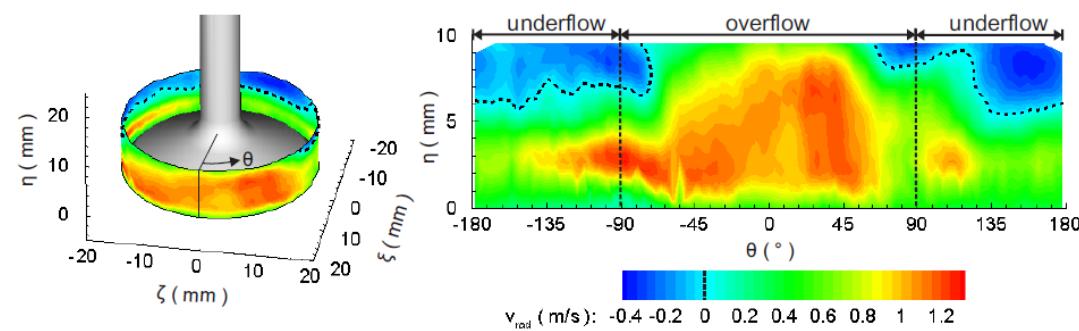
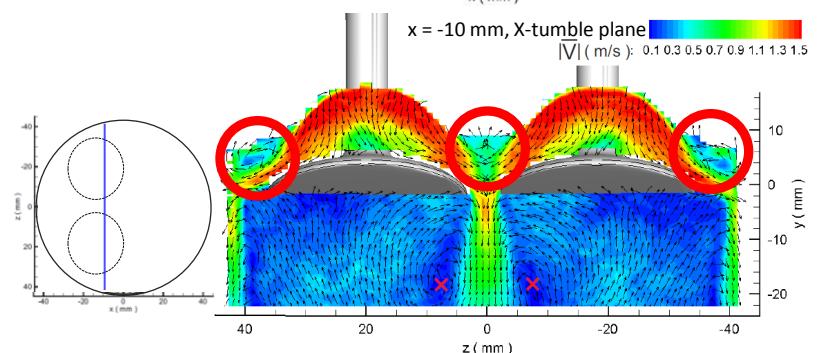
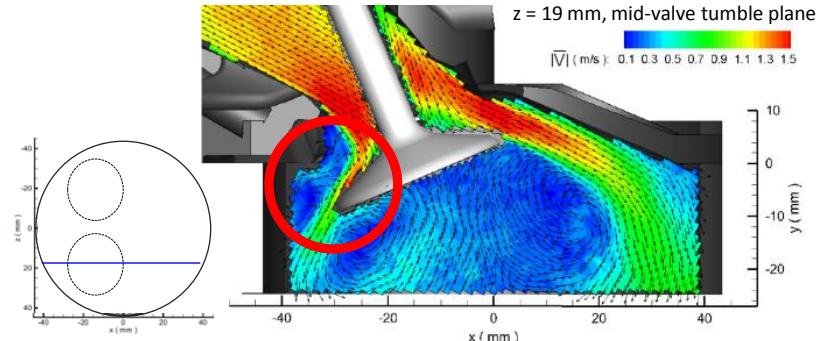
- Intake system & cylinder

■ Recirculation zones

- Intake geometry
- Valve flow through valve curtain
- Volumetric efficiency csq
- Cyclic flow behavior

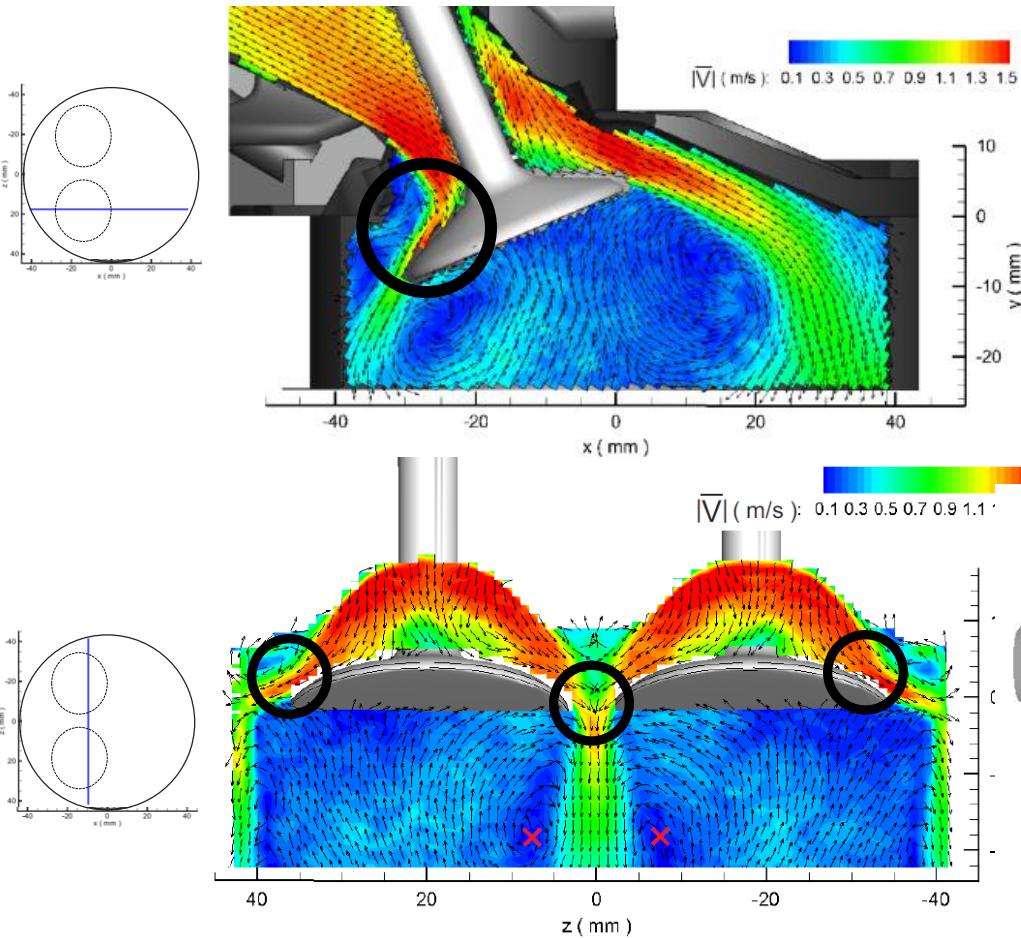
■ Improve understanding of intake flow

- Simulation efforts underway
- Fine grid spacing in intake geometry

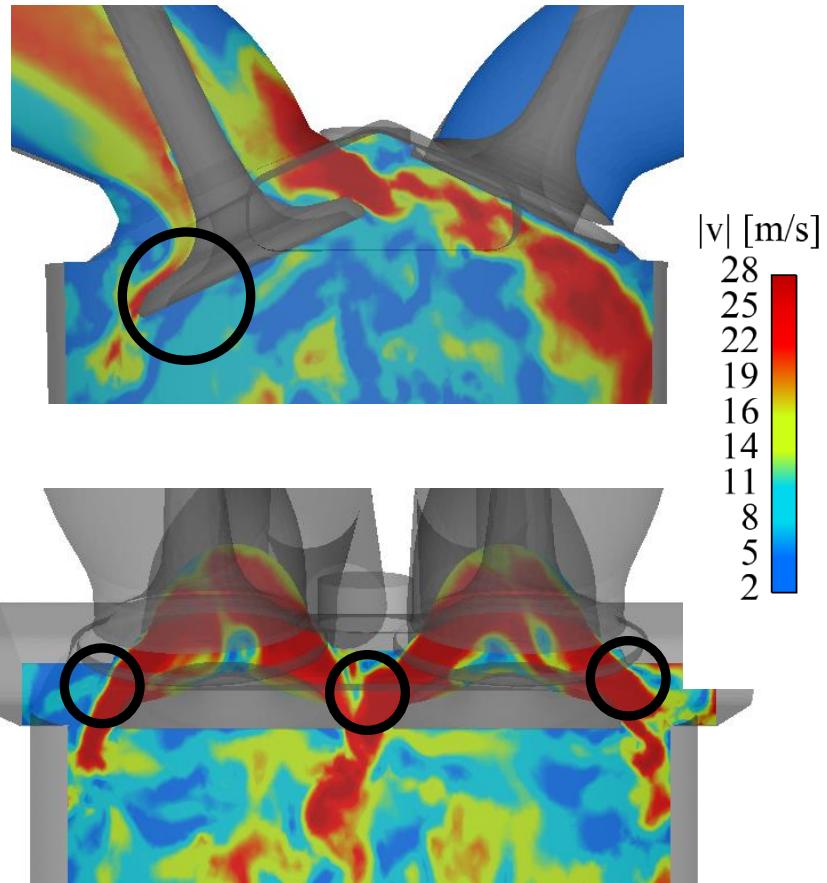


Influence of Intake Flow

Exp -TUD

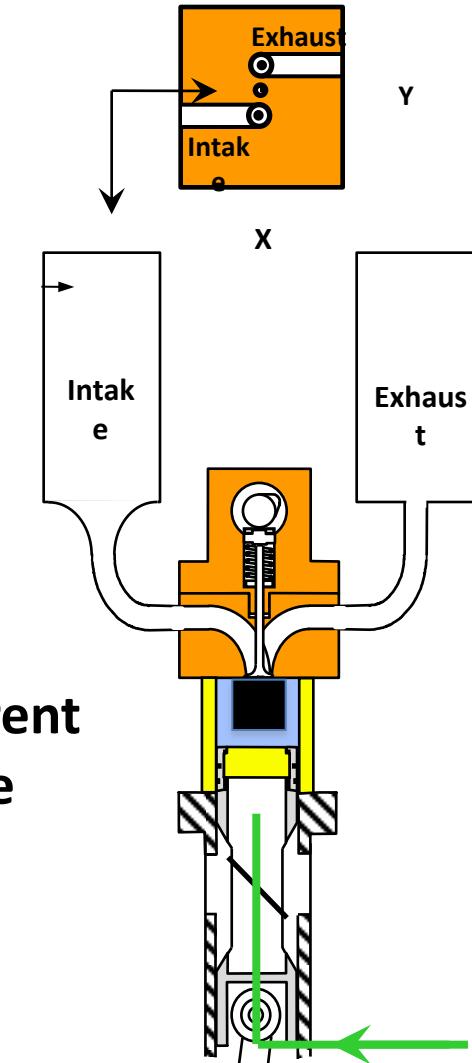
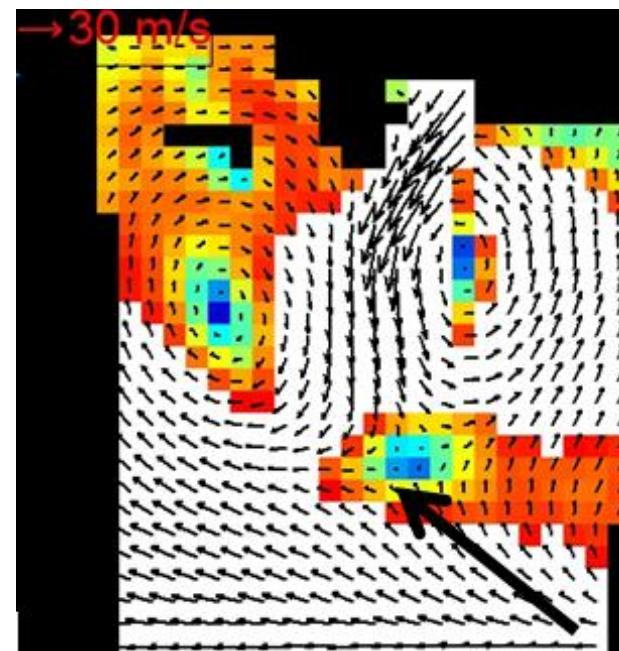
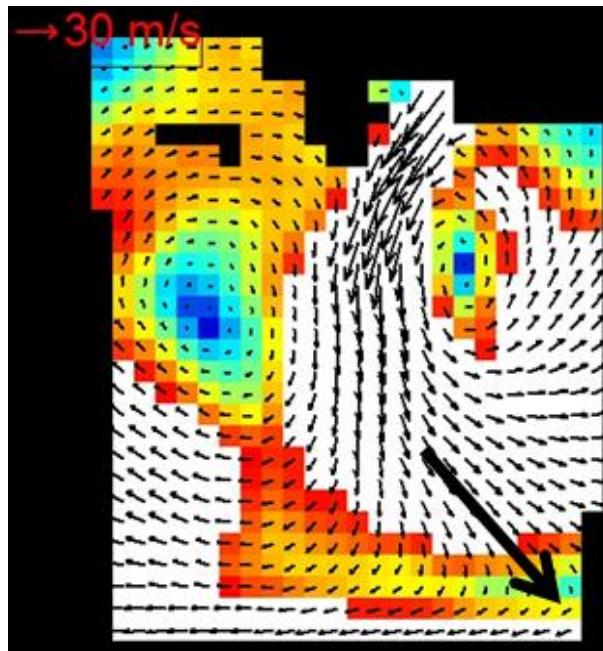


LES - SGEmac



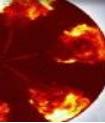


Flow Pattern (TCC – Univ Michigan)



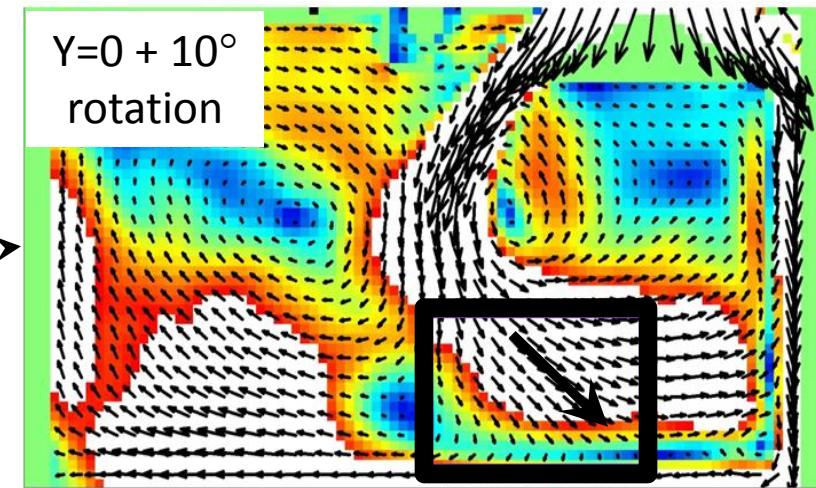
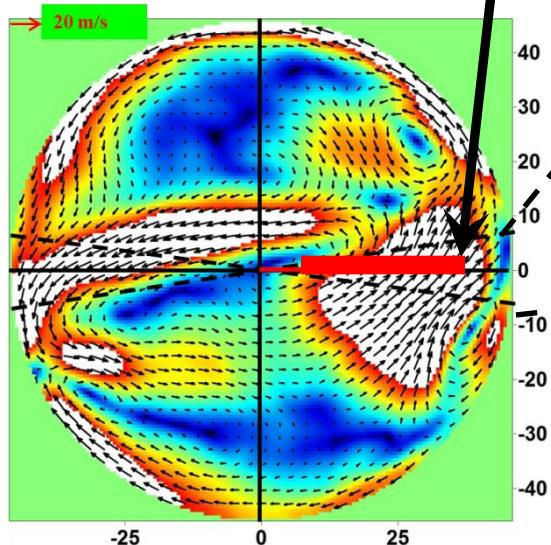
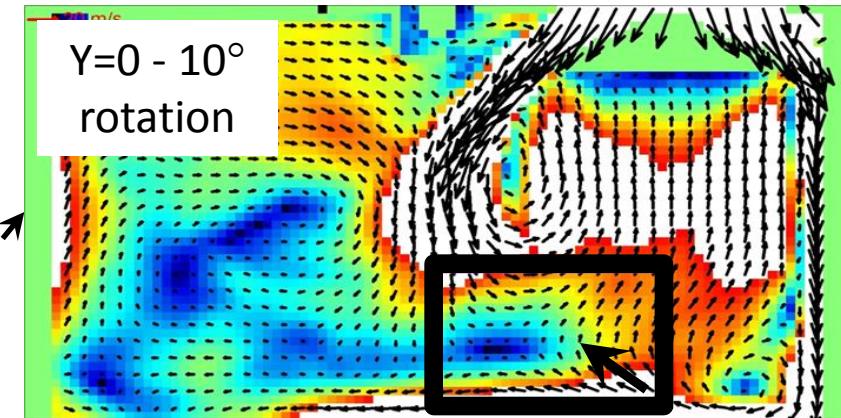
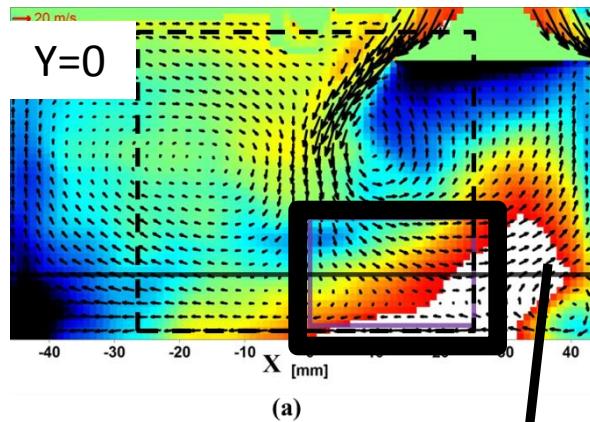
- At mid-intake stroke, ensemble-averages from different 70-cycle samples show flow structures with opposite direction
- Measurements show both flow patterns exist
 - Appearance is sample dependent

• "Effect of Boundary Conditions on Intake Flow Patterns in a Motored Spark Ignition Engine", Abraham et al. submitted to IJER, 2014



Flow Pattern (TCC – Univ Michigan)

Use 3-D LES data, sampled at rotated planes,
to identify the reason for flow CCV





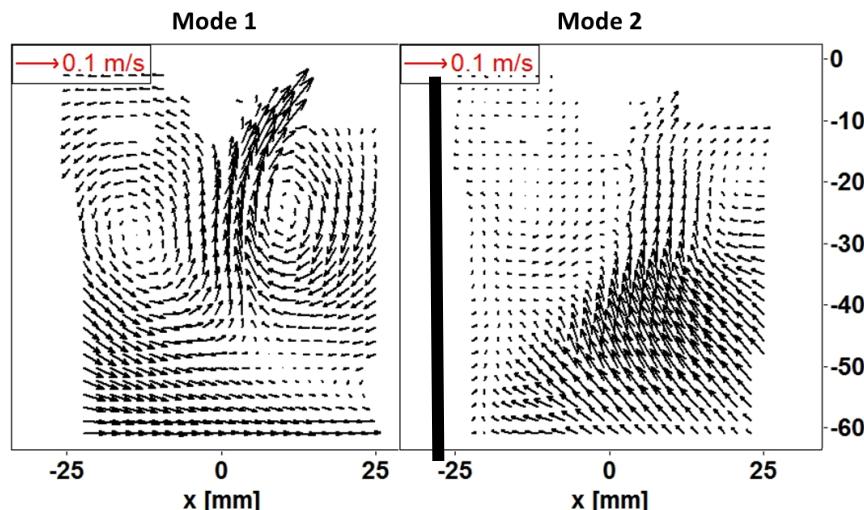
Flow Pattern (TCC II – Univ Michigan)

Use conditional sampling of POD modes to correlate flow structure

with: ■ Intake Port Pressure → No Correlation

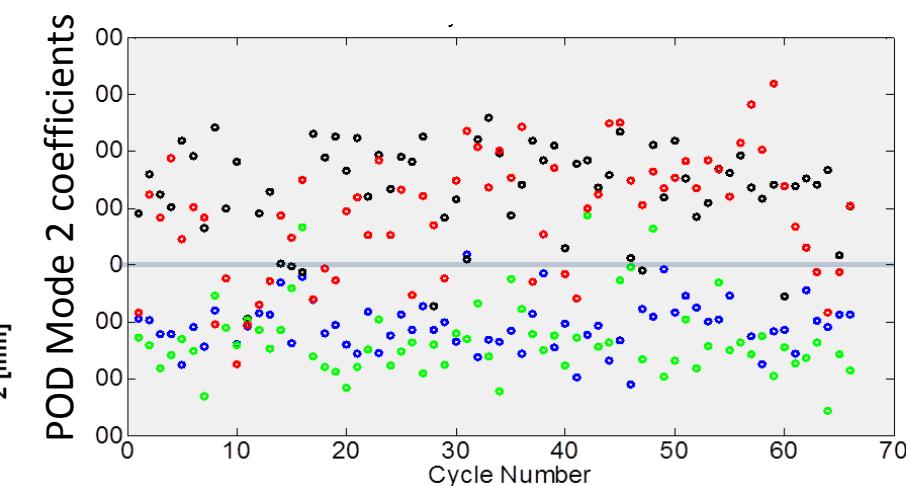
■ Lateral valve oscillation → Very weak correlation

■ RPM changes → Inconclusive

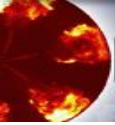


POD Mode 1
dominated by
intake jet &
entrainment vortices

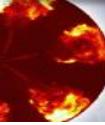
POD Mode 2
dominated by Lower
Right-Hand, flow
structure



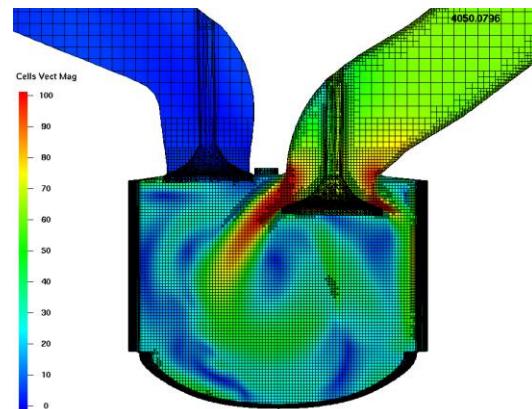
#1, SS 1 #1, SS 2 #2 #3
Mode 2 coefficients correlate with
direction of LRH flow structure



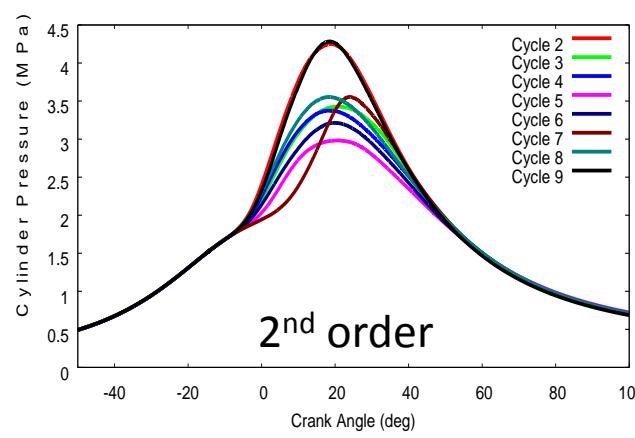
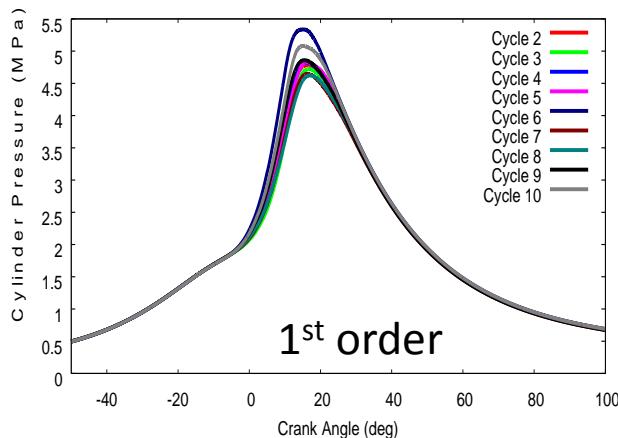
2. Fired operation



Direct-Injection Spark Ignited Example

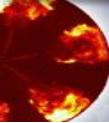


Bore	101.6 mm
Stroke	100.0 mm
Connecting Rod	180.0 mm
Compression ratio	9.2:1
Number of Valves	4
Start of Injection	-220 deg. ATDC
Spark Timing	-15 deg. ATDC
Engine Speed	3000 RPM
Equivalence Ratio	1

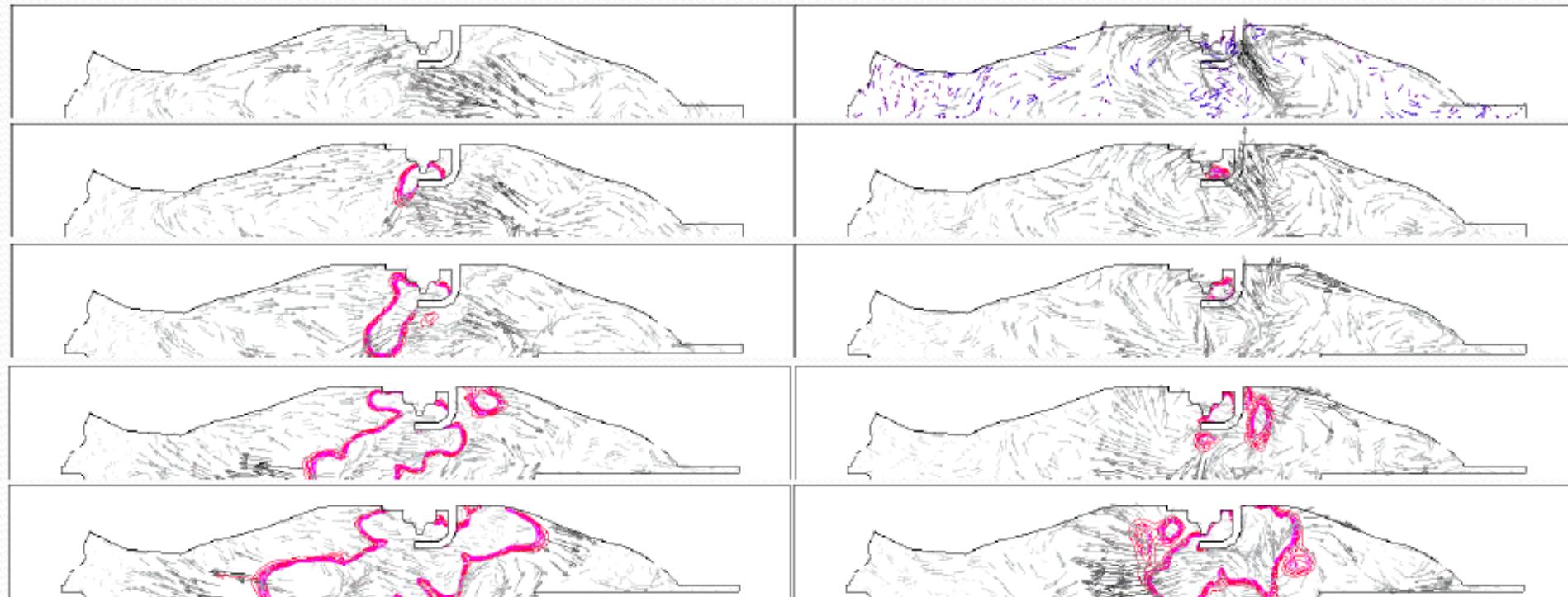


CCV exist in RANS simulations if the numerical viscosity is sufficiently minimized

	<u>First Order</u>	<u>Second Order</u>
IMEP (bar)	9.9	9.2
COV of IMEP	1.8	3.9

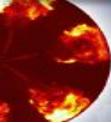


Combustion progress (UNIMORE) LES computations



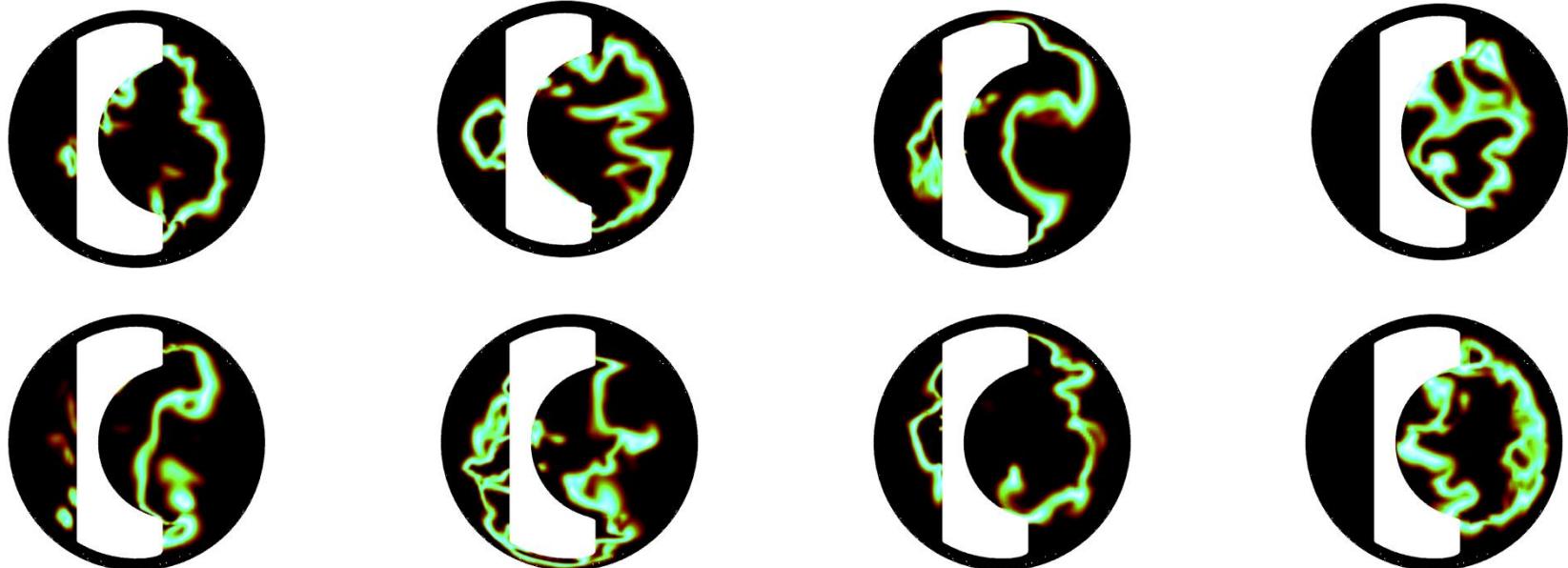
Difference in flame propagation between the fastest cycle (left) and slowest one (right)





Combustion progress (CTU Prague)

LES computations



- Difference in flame propagation
- Critical parameters are:
 - combustion speed - driven by turbulence level
 - Ignition delay – initial flame kernel development

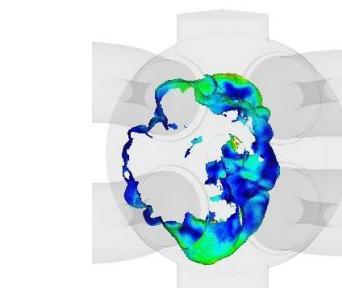
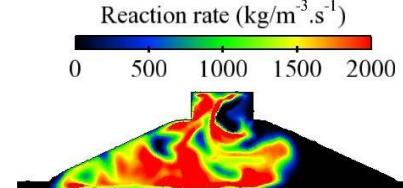
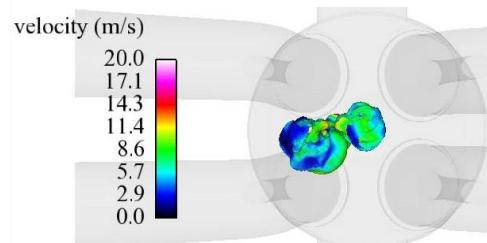
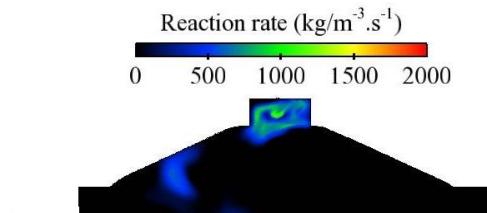




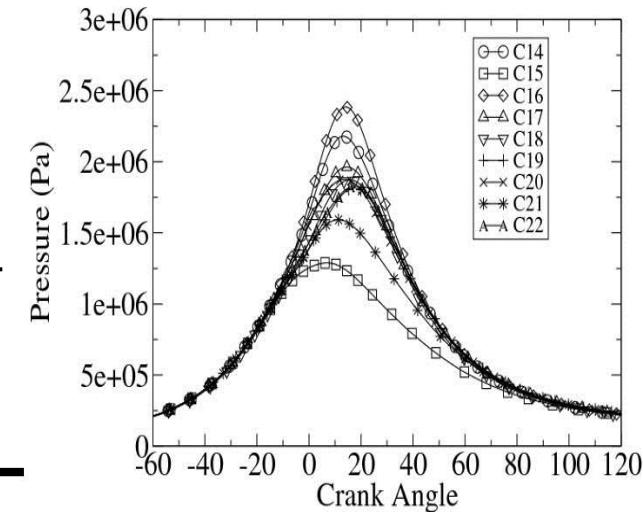
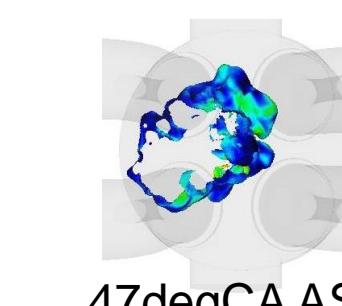
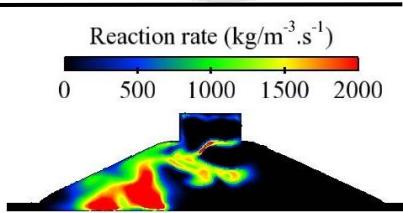
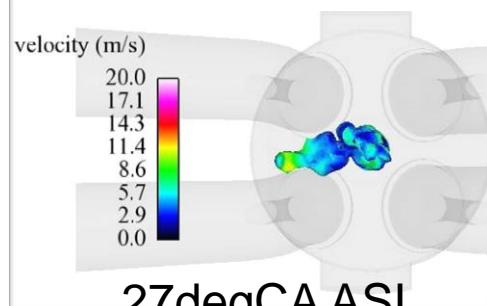
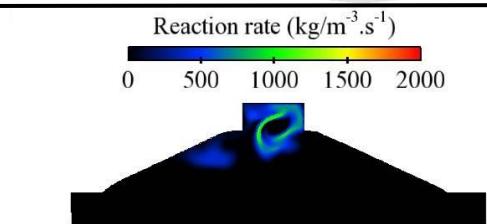
Combustion progress (SGEmac IFP)

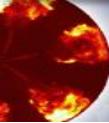
LES computations

Fast Cycle



Slow Cycle

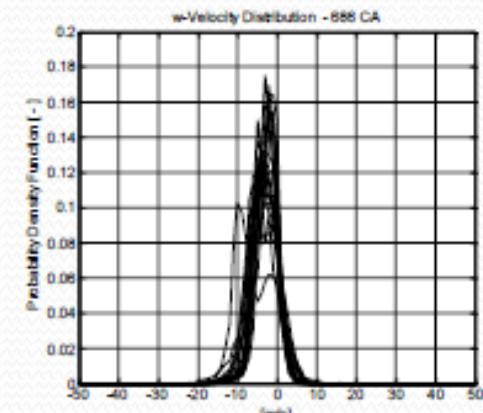
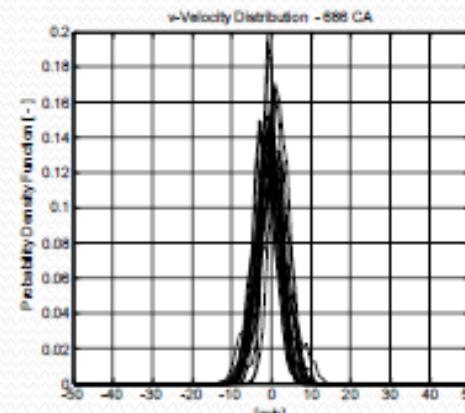
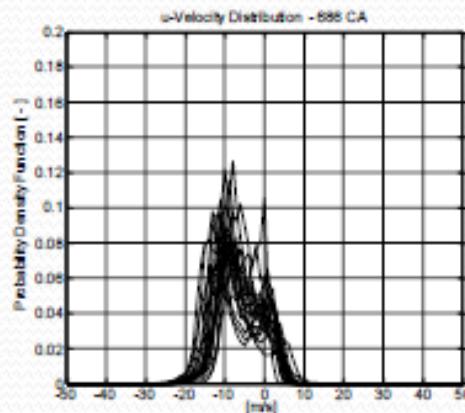




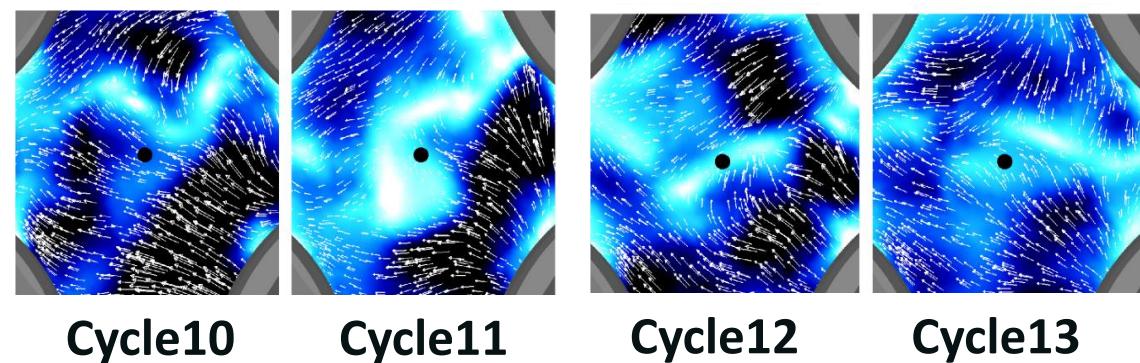
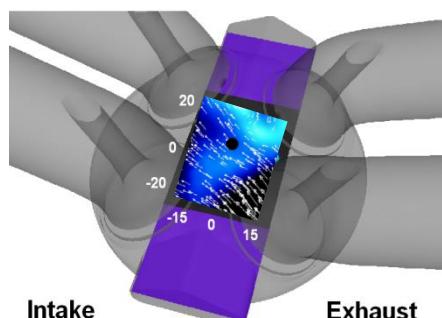
Flow fluctuations close to the spark plug @ spark timing (LES IFP, LES UNIMORE)

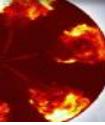


PDF of flow component around the spark during ignition



Velocity statistic around the spark during ignition



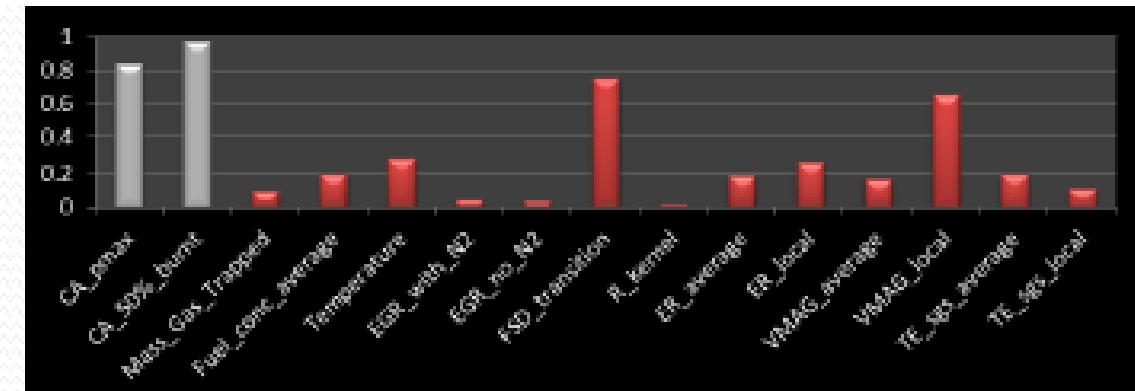


Cross-correlation coefficient – Both 0D and Fully 3D (UNIMORE)

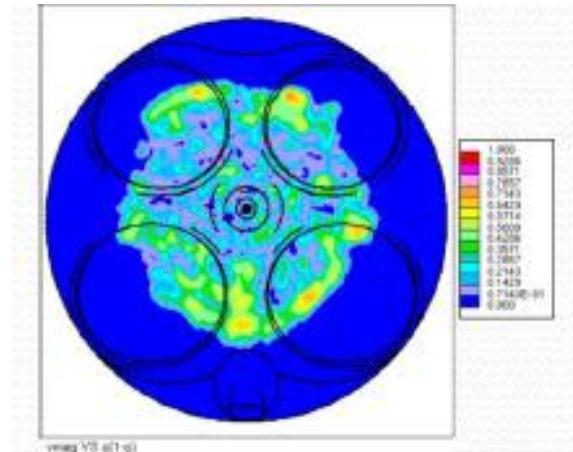
LES computations

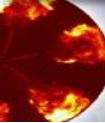


Correlation Coefficient (Pmax, Yj)



Correlation Coefficient spatial distribution

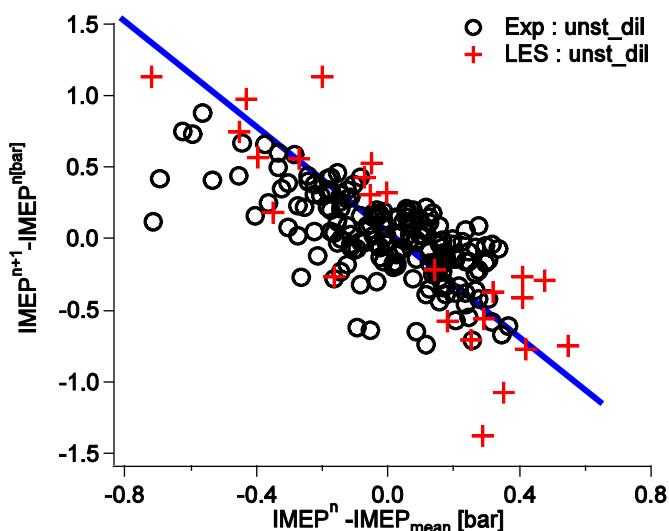




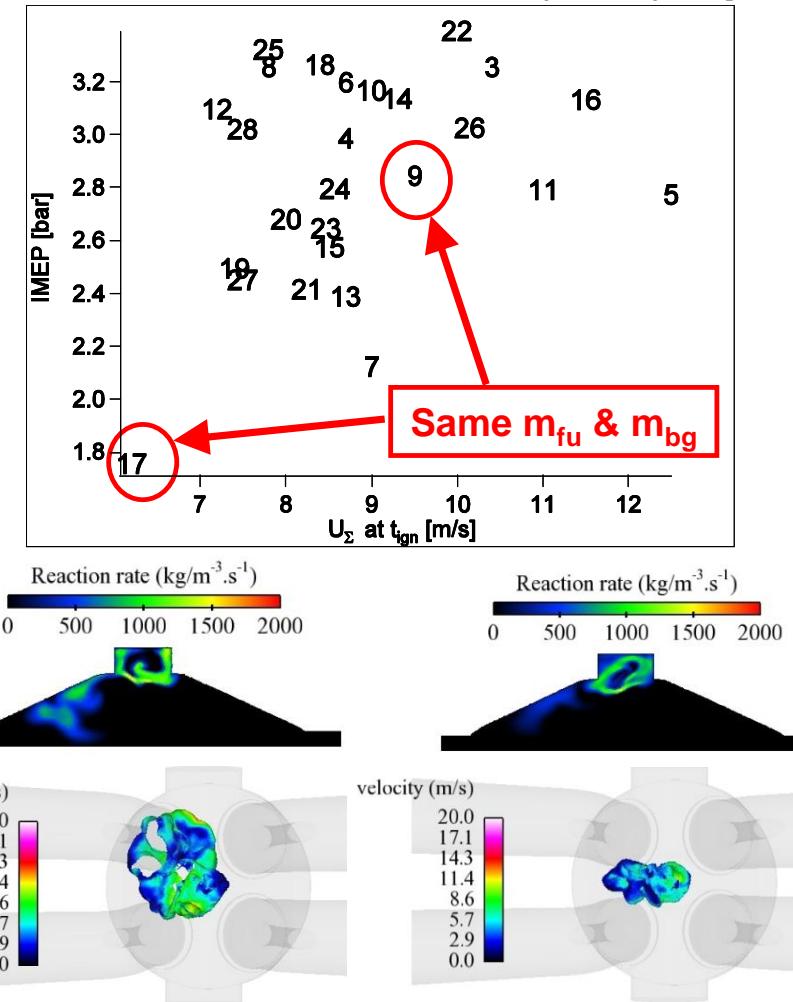
IMEP correlation (IFP)

LES computations

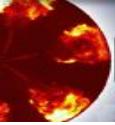
Variations of IMEP from C to C



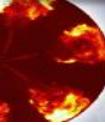
IMEP vs convection at spark plug



- Important effect of the flow properties on the flame development and so on CCVs
 - Turbulence structure
 - Turbulence intensity
 - Turbulence scales



3. New modeling tools



How to introduce CCV in 1D modeling

Naturally described by codes (@ 1st order)

Variations of:

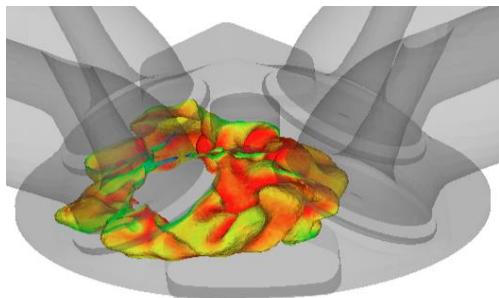
Intake system

- Turbulence
- Acoustics
- Op. conditions

- Trapped mass
- EGR rate, temperature
- Fresh mixture composition

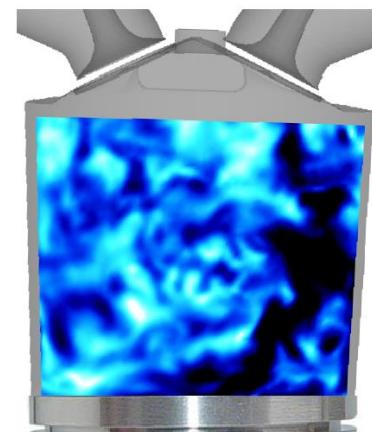
Exhaust system

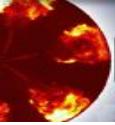
- Turbulence
- Acoustics
- Op. conditions



- Large scale flow patterns
- Small scale turbulence
- Conditions at spark plug
- In-cylinder temperature

Needs in-cylinder phenomena details

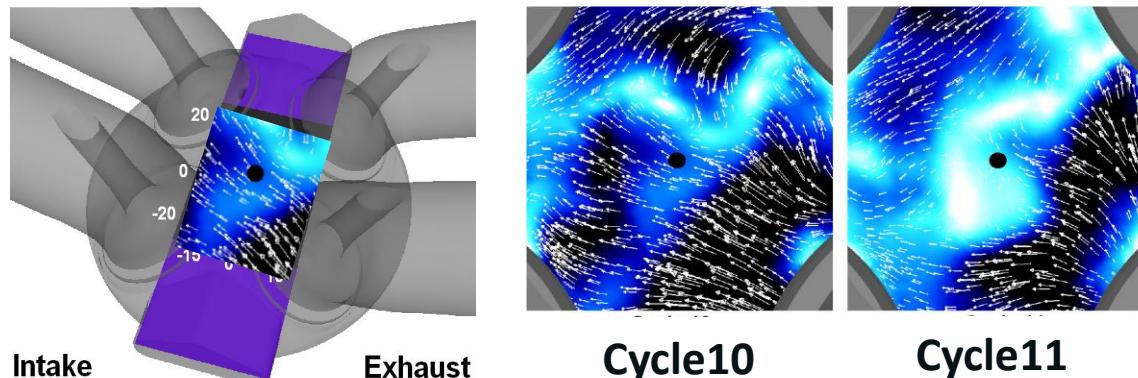




Strategy

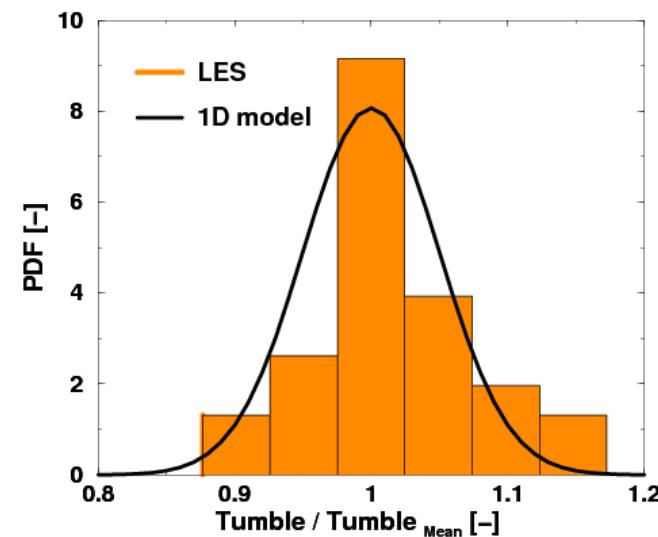
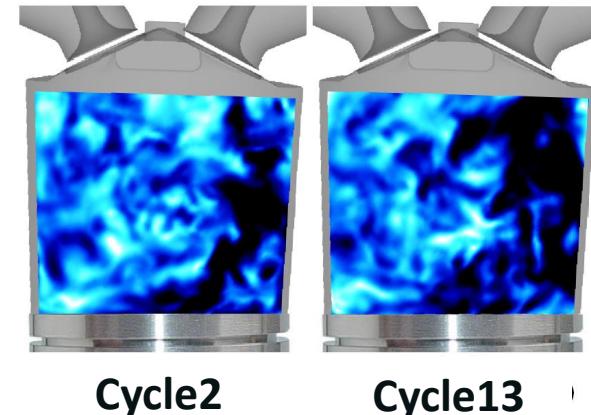
Dedicated post-processing of cold flow LES

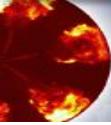
- Turbulent scales @ spark timing (I_t)
- Tumble number @ IVC (large scale kinetic energy – K)
- Velocity fluctuations close to the spark plug @ spark timing



Tumble motion study

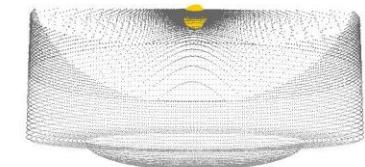
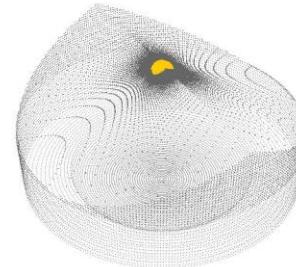
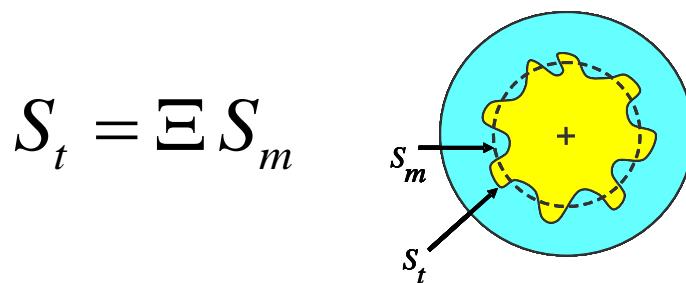
- Gaussian shape of the probability density function (LES) @ IVC





The CFM-CCV 1D model^[1]

- Two-zone model (fresh/burnt gases)
- Based on CFM 1D model^[2]
- Flame surface:

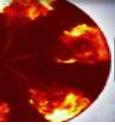


$$\frac{1}{\Xi} \frac{d\Xi}{dt} = \Gamma(u'/U_l, l_t/\delta_l) \frac{u'}{l_t} \left(\frac{\Xi_{equ} - \Xi}{\Xi_{equ} - 1} \right) - \frac{2}{r_{bg}} (1 + \tau) (\Xi - 1) U_l$$

- Turbulence model for
 - u' : turbulence fluctuations
 - l_t : turbulence integral length scale

[1] Pera et al. SAE 2012-01-0127

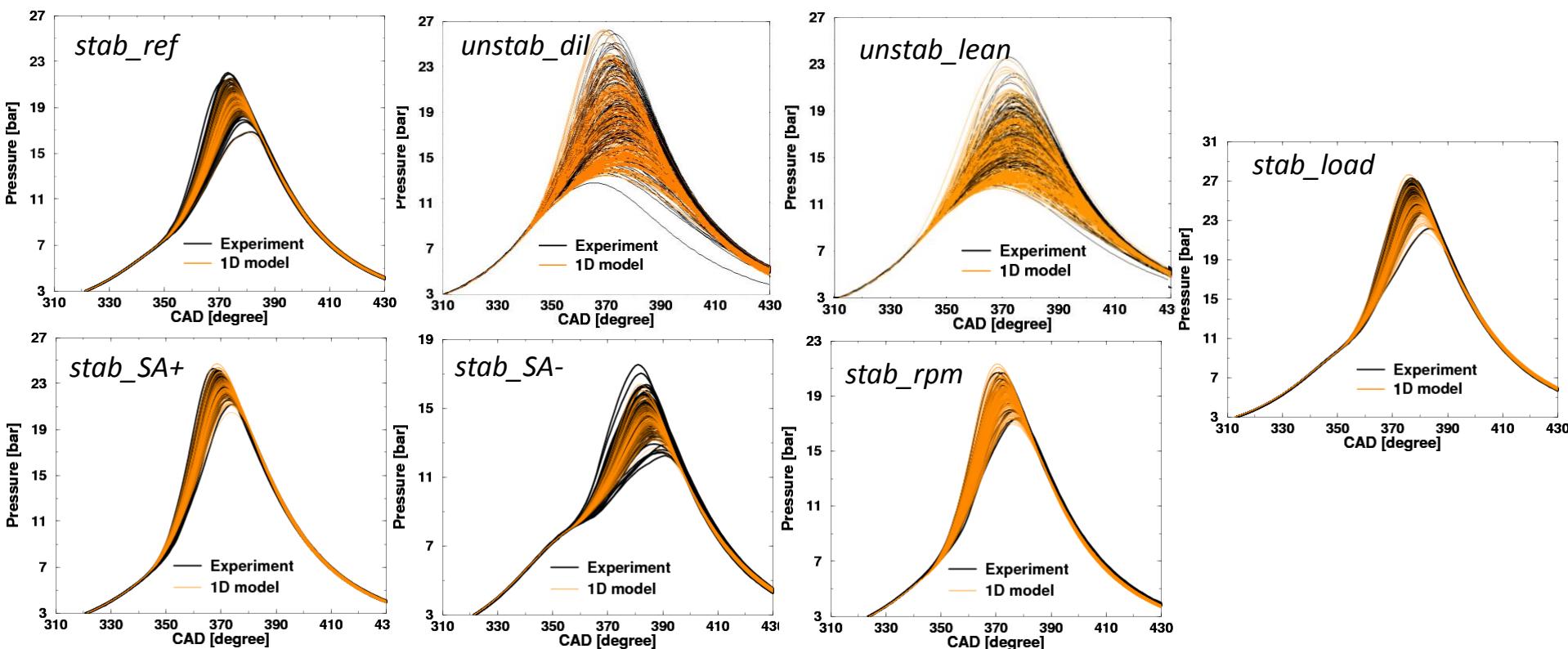
[2] Richard et al. (2009) Oil Gas Sci Technol 64(3)

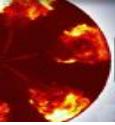


The CFM-CCV 1D model^[1] – Validation on the SGEmac database

■ Cylinder pressure envelop results

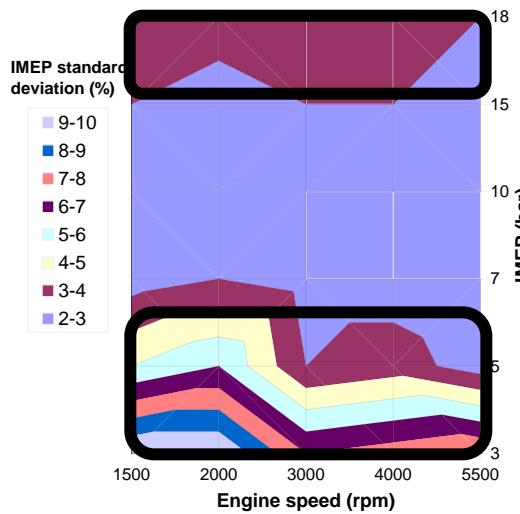
- Simulation of 100 cycles for stable 200 cycles for unstable conditions
- The same relative perturbations are used for all engine speed/load





Engine operation stability map

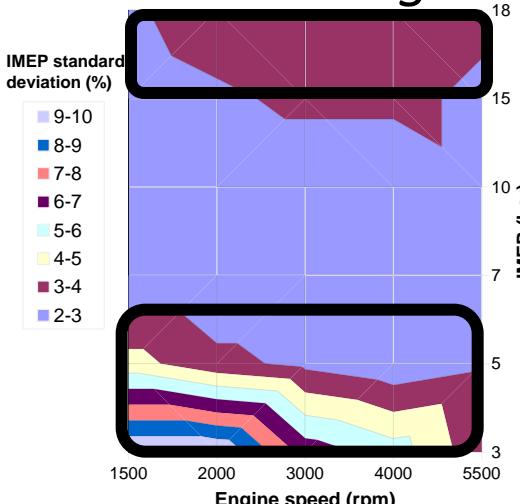
Experimental map



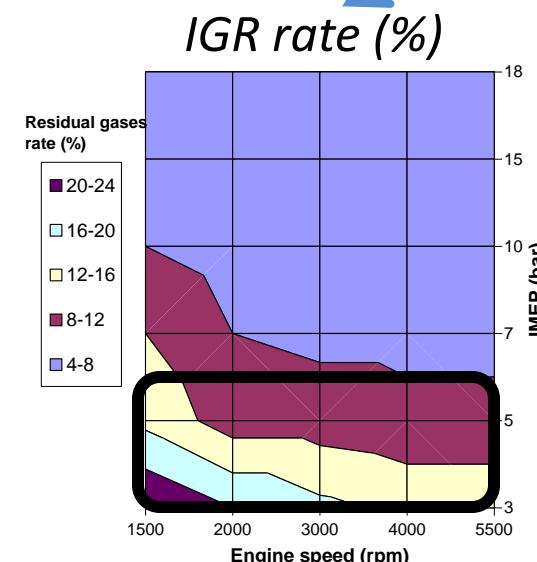
Stable and **unstable** zones are predicted for all conditions

Instability may be linked to chemistry modification : dilution or high enrichment

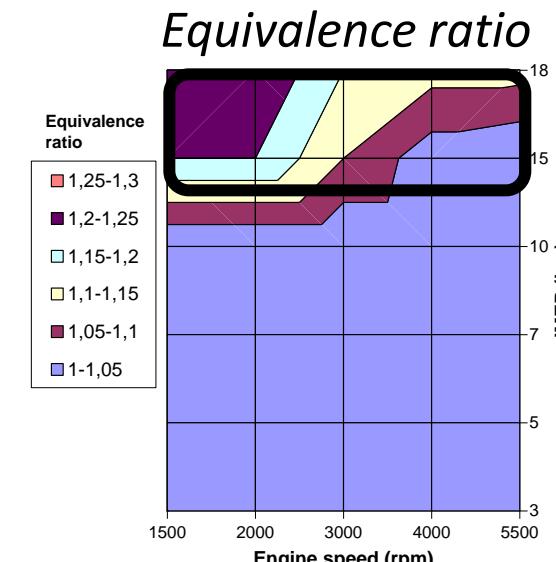
Modeling

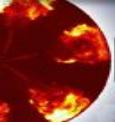


IGR rate (%)

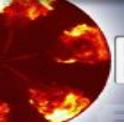


Equivalence ratio



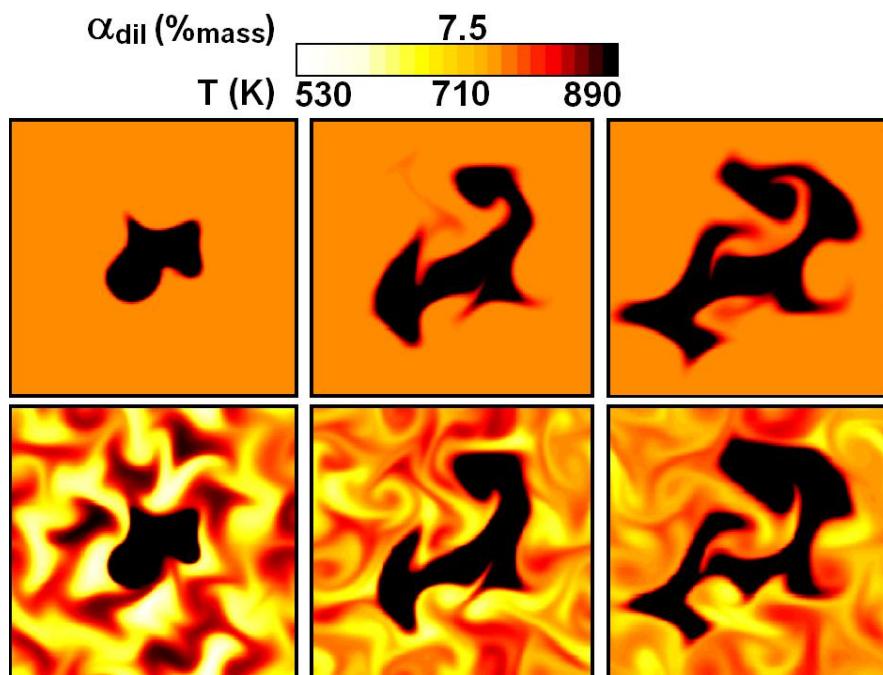
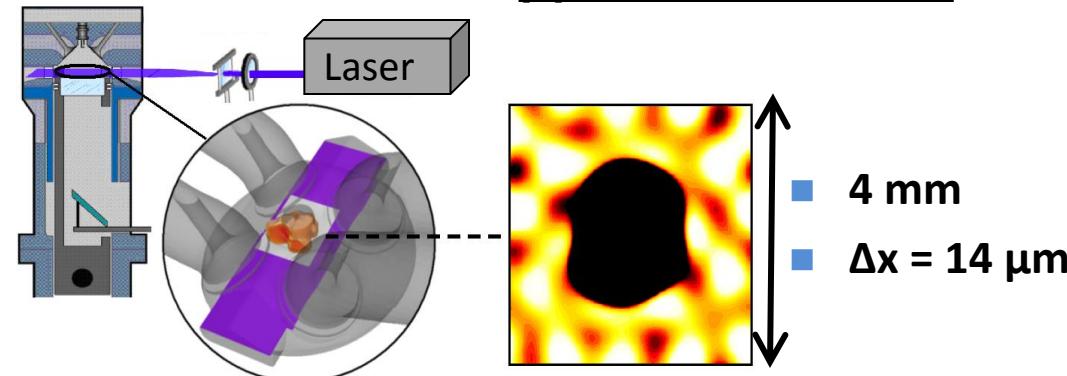


4. Perspectives



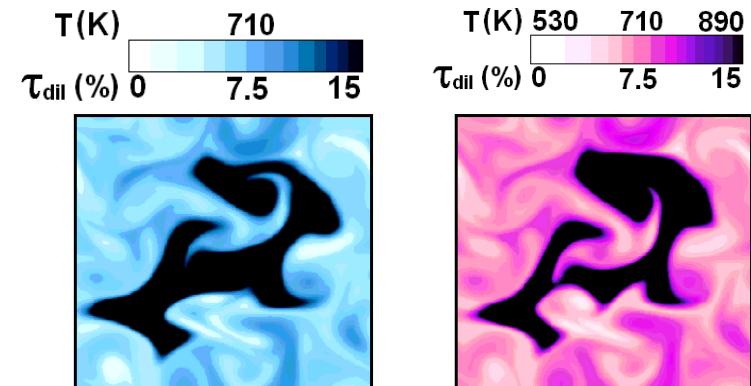
DNS of early flame propagation for CCV understanding^[3]

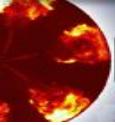
[3] Pera et al., FTaC 2014



- Temperature heterogeneity could highly modify flame shape
- Effect of temperature is dominant over that of dilution

Based on SGEmac exp.
(Unstab-Lean op. pt)



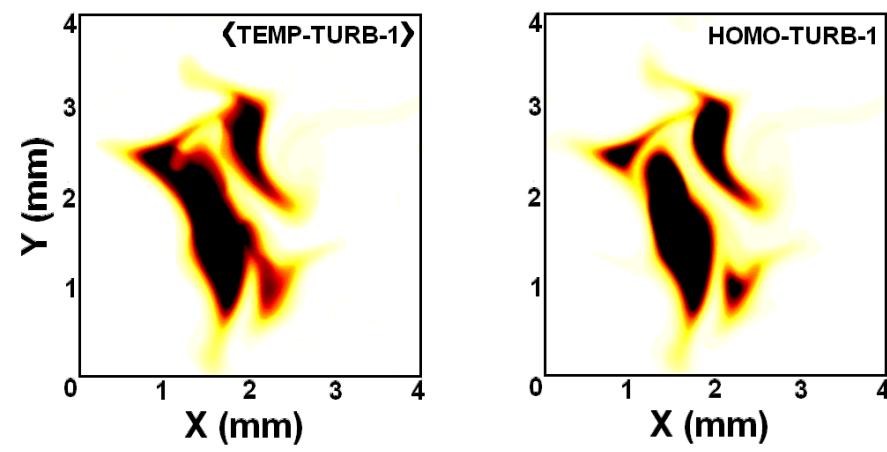
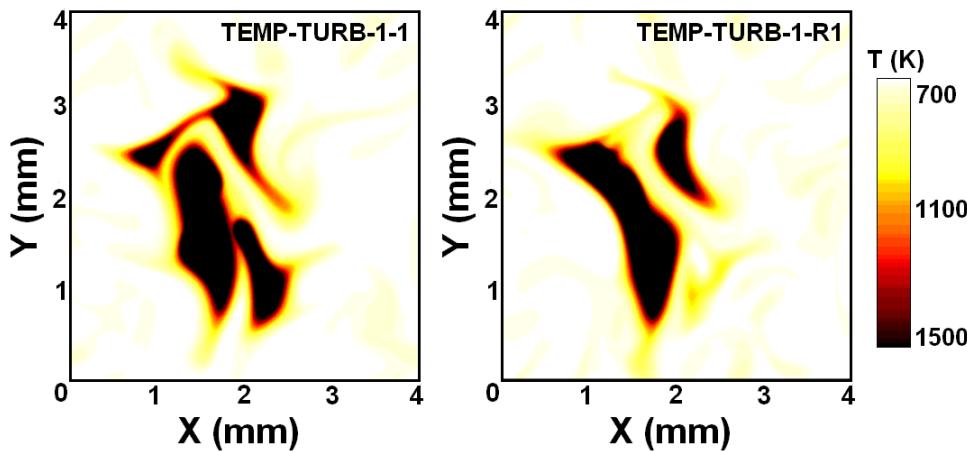


DNS of early flame propagation for CCV understanding^[3]

4 realizations
≈ 4 engine cycles

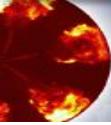
Ensemble average
(4 cycles)

Modeling
(RANS or LES)



- Error in flame shape if heterogeneities (temperature / dilution) are not explicitly accounted for
- RBG Heterogeneities contribute to quench the flame
 - Modelling?

[3] Pera et al., FTaC 2014



Contributions

1. Motored operation

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3. New tool modeling,

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4. Perspective,

All